Gas-Liquid Solubilities of Carbon Monoxide, Carbon Dioxide, Hydrogen, Water, 1-Alcohols $(1 \le n \le 6)$, and *n*-Paraffins $(2 \le n \le 6)$ in HexaJecane, Octacosane, 1-Hexadecanol, Phenanthrene, and Tetraethylene Glycol at Pressures up to 5.5 MPa and Temperatures from 293 to 553 K

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The gas-liquid solubilities of the solutes carbon monoxide, carbon dioxide, hydrogen, water, ethane, propane, pentane, hexane, methanol, ethanol, 1-propanol, 1-butanol, 1-pentanol, and 1-hexanol in the solvents tetraethylene glycol, hexadecane, octacosane, 1-hexadecanol, and phenanthrene were measured as a function of temperature. The solutes are all reactants or products relevant for synthesis gas conversion into alcohols and/or hydrocarbons. The solvents are seen as potentially attractive for synthesis gas conversion via gas-slurry processes. Experimental conditions varied between 293 and 553 K and 0.06 and 5.5 MPa, covering typical process conditions for synthesis gas conversion. The total set of experimental results consists of 1533 gas-liquid solubilities divided over 60 binary systems. As far as we know hardly any of the gas-liquid solubilities from this set have been reported previously in the literature. Where literature data are available, a comparison is made with our data. This comparison always shows an agreement within the calculated experimental errors with an average deviation of 7.6% and a maximal deviation of 15.0%.

Introduction

At temperatures between 473 and 673 K and pressures between 2 and 10 MPa, synthesis gas can be converted toward methanol, fuel-methanol (a mixture of methanol and higher alcohols), or a mixture of hydrocarbons (Fischer-Tropsch synthesis), depending on the type of heterogeneous catalyst applied. Gas-solid packed bed reactors are usually applied (1, 2) but new gas-slurry processes gain attention (3, 4). Then the selection of the inert, high-boiling solvent is important, and the magnitude of the gas-liquid solubilities of both the reactants and the products in this liquid can be a crucial criterion.

Experimental data on the solubilities of reactants and products in synthesis gas conversion in such liquids are very scarce in the open literature, particularly at typical synthesis conditions, which involve high pressures and high temperatures. The aim of this study is to measure the solubilities of these reactants and of the major products in several potentially attractive liquid solvents over a wide temperature range.

Selection of Solutes and Solvents

In the Fischer-Tropsch, the methanol, and the methanol-higher alcohol synthesis, the most relevant components are (1) synthesis gas reactants (carbon monoxide, carbon dioxide, and hydrogen); (2) in methanol synthesis, the product (methanol); (3) in methanol-higher alcohol synthesis, also higher linear and branched alcohols; (4) both in Fischer-Tropsch synthesis and as side products in the methanol-higher alcohol synthesis, linear olefins and paraffins; and (5) the unavoidable side product of synthesis gas conversion (water).

As solutes we selected all the methanol synthesis components (carbon monoxide, carbon dioxide, hydrogen, wa-

Table 1. Pur Used in This	rity and Source Study	or Origin of	the Chemicals

name	formula	source	purity (mass %)		
nitrogen	N ₂	Hoekloos	> 99.995		
	Solutes				
hydrogen	H_2	Hoekloos	>99.995		
carbon monoxide	CÔ	Hoekloos	>99		
carbon dioxide	CO_2	Hoekloos	>99.9		
ethane	C_2H_6	Hoekloos	>99		
propane	C_3H_8	Hoekloos	>99.5		
pentane	C_5H_{12}	Merck	>99		
hexane	$C_{6}H_{14}$	Merck	>99		
methanol	CH ₃ OH	Merck	>99.8		
ethanol	C_2H_5OH	Merck	>99.8		
1-propanol	1-C ₃ H ₇ OH	Merck	>99.5		
1-butanol	1-C₄H ₉ OH	Merck	>99.5		
1-pentanol	$1-C_5H_{11}OH$	Merck	>99		
1-ĥexanol	$1-C_6H_{13}OH$	Merck	>98		
water, double distilled	H_2O		>99.9		
	Solvents				
tetraethylene glycol	$C_8H_{18}O_5$	Merck	>97		
phenantrene	$C_{10}H_{14}$	Merck	>98		
ĥexadecane	$C_{16}H_{34}$	Merck	>99		
1-hexadecanol	1-C16H33OH	Merck	>97		
octacosane	C ₂₈ H ₅₈	Merck	>97		

ter, and methanol) and further a set of linear alcohols (ethanol, propanol, 1-butanol, 1-pentanol, and 1-hexanol) and a set of linear paraffins (ethane, propane, pentane, and hexane), representing the most polar and apolar products in synthesis gas conversion, respectively. Solvents were selected on the basis of varying specific properties such as polarizability (phenanthrene), apolarity (hexadecane and octacosane), and polarity (1-hexadecanol and tetraethylene glycol). See Table 1 for the purity and source or origin of the chemicals used in this study.

Experimental Section

Experimental Method. The experimental method is similar to that of Olsen (5), Cukor and Prausnitz (6), and

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Figure 1. Experimental arrangement: (1) stainless steel autoclave, (2) temperature control unit including heating element, (3) interface card, (4) personal computer, (5) low- or high-pressure transmitter, (6) valve, (7) Pt-100 resistance thermometer, (8) magnetic stirring unit, (9) hole, (10) valve, (11) valve, (12) stainless steel supply cylinder, (13) Mettler balance, (14) valve, (15) manometer, (16) syringe, (17) valve, (18) digital pressure indicator, (19) vacuum pump.

Graaf et al. (7). Known amounts of the two components were locked-up in a vessel of known volume. After the temperature was increased stepwise, the system was allowed to reach equilibrium. These equilibria are characterized by a set of primary measured values: P, T, V_{sys} $(T_0), n_1^T$, and n_2^T , where P = pressure (MPa), T = temperature (K), $V_{sys}(T_0) =$ vessel volume (m³) at $T = T_0$ (293 K), n^T is the total number of moles locked-up in the vessel, and 1 and 2 refer to the solute and solvent, respectively. The gas-liquid solubility of component 1 is characterized by the mole fractions of component 1 in the liquid phase and the gas phase, x_1 and y_1 , respectively. These two quantities were calculated indirectly from the primary measured quantities as described below.

Experimental Arrangement. A scheme of the experimental arrangement is given in Figure 1. See Figure 2 for details on the stainless steel autoclave (1), which was magnetically stirred by three six-bladed turbine stirrers placed on a common shaft and provided with four radial baffles, ensuring rapid physical equilibrium between the gas and liquid. At least one stirrer rotated in the liquid. The stirring unit had a very small dead volume of about 10 cm³. To avoid both condensation of the solute in this dead volume and irreversible demagnetizing of the magnets, which occurs at T > 473 K, the temperature of the magnet chambers was controlled at 448 K. The temperature inside the autoclave was measured with a Pt-100 resistance thermometer (7) (Tempcontrol, type four-lined Pt-100, range 273-773 K). The Pt-100, including the electronic transducing unit, was calibrated using a standard resistance bank, melting ice, and boiling water. The estimated error of the temperature measurement was ± 0.3 K (including reproducibility and systematic effects due to the calibration). The autoclave was further connected to a pressure device with an effective dead volume of 5 cm³. This unit contained either a low- (5) (Druck, type PDCR 910, range 0-1 MPa) or a high-pressure transmitter (5) (Druck, type PDCR 910, range 1–20 MPa), depending on the kind of solute. To ensure an accurate, reproducible pressure measurement, the pressure transmitters were kept at a constant temperature of 293 K. The pressure



Figure 2. Detailed sketch of the autoclave.

transmitters, including the electronic transducing units, were calibrated with accurate manometers [15 (Wiegand, type 342.11, 0–16 MPa, class 0.1, inaccuracy ± 0.01 MPa) and 18 (Vacuubrand, 0-0.12 MPa, type 220, inaccuracy ± 0.0005 MPa)]. The estimated error of the pressure measurement was ± 0.0015 MPa for the low- and ± 0.015 MPa for the high-pressure transmitter (including reproducibility and systematic effects due to calibration). Condensation of solutes was avoided by separating the pressure transmitter from the gas phase by a seal of silicon oil in a narrow tube (1.6 mm) to minimize the contact surface with the gas phase. By connecting the seal to a small volume of high-pressure carbon dioxide and measuring the pressure as a function of time, it could be experimentally shown that possible inaccuracies by dissolution of the gas in the sealing oil or by evaporation of the sealing oil were negligible. From the top of the autoclave down to about 2 cm below the oil seal the pressure device was thermostated electrically at 473 K to avoid possible condensation of solutes. The autoclave was also connected to a highpressure, high-temperature valve (10), which could be provided with a septum to inject liquid solutes. To feed gaseous solutes, the valve could be connected to a gas supply cylinder (11-13). The autoclave was electrically heated. To ensure good isothermal conditions, a jacket of aluminum was placed between the autoclave wall and the heating element and both the heating element and the top and bottom of the autoclave were thermally insulated by glass wool. All seals were of either copper or stainless steel (see also Figure 2), and precautions were taken to avoid overheating of the magnets of the stirring unit and the pressure transmitters. Therefore, the experiments could be carried out at relatively high temperatures in the autoclave (up to 553 K in this study) without encountering specific practical problems.

Estimation of the System Volume. The effective system volume was measured at $T_0 = 293$ K by filling the system with a known amount of pure nitrogen and subsequently measuring the pressure increase with a manometer (15). The mass of nitrogen added followed from the differential mass of the supply cylinder (12), ΔW_{supply} , measured with a balance (13) (Mettler, type PC 4400, inaccuracy ± 0.01 g per reading). This procedure was

repeated 10 times. The system volume, $V_{sys}(T_0)$, was calculated from the nitrogen mass balance:

$$V_{\rm sys}(T_0) = \frac{RT_0 \Delta W_{\rm supply}}{(P_1 Z_1^{\rm V} - P_0 Z_0^{\rm V}) M_{\rm N_2}} \tag{1}$$

where P_0 , P_1 and Z_0^V , Z_1^V are the pressures and compressibility factors before and after adding nitrogen, respectively, M_{N_2} is the molar mass of nitrogen, and R is the gas constant (=8.314 J mol⁻¹ K⁻¹). The compressibility factors Z_0^V and Z_1^V were obtained from *Gas Encyclopaedia* (8). The system volume was taken as the average of all measurements to give $V_{sys}(T_0) = (974 \pm 2) \times 10^{-6}$ m³. The error included both reproducibility and systematic effects.

Measurement of Gas-Liquid Equilibria. The clean autoclave was filled with an amount of solvent accurately measured from the differential mass of the autoclave (Mettler balance, type PM 46, inaccuracy ± 0.1 g per reading). While stirring, the solvent was degassed with a vacuum pump (19) (valves 10 and 17 open, valves 6 and 14 closed). The degassing was considered to be complete if, after stopping pumping, the pressure increase in time stayed below 4 kPa. The amount of injected liquid solutes was measured from the differential mass of the syringe (Mettler balance, type H10, inaccuracy ± 0.0001 g per reading). Gaseous solutes were fed from a supply cylinder (12) (valves 6, 10, 11, and 14 open, valve 17 closed). After valve 10 was closed and stabilization of the pressure as indicated by manometer 15, the amount of solute fed to the autoclave could be accurately calculated from the differential mass of the supply cylinder (balance 13), taking into account the amount of gas entrapped in the volume between valves 10, 11, and 17. The volume of this system (38 cm^3) was measured the same way as described above for the vessel volume. The amount of gas entrapped in this section was calculated from the observed pressures before and after feeding the gaseous solutes. For a particular, accurately known, mixture present in the autoclave, a set of experiments with varying temperature was carried out at a rotational stirrer speed of 23.3 rps. Such sets of experiments were run automatically under an in-housedeveloped Turbo-Pascal computer program. The temperature control of the autoclave (2) and the data acquisition with respect to pressure and temperature were automated using a personal computer (4) linked to the equipment via an interface card (3). The temperature control was realized via a PID algorithm. The set point of the temperature control unit was increased with steps of approximately 5 K. Equilibrium was established at these temperatures and could be detected by the computer program as follows: if five subsequent pressure and temperature measurements. measured within a time interval of at least 10 min, were constant within 0.3 K and 0.001 or 0.01 MPa, for the lowpressure and the high-pressure transmitters, respectively, without showing any trends with time, the gas and liquid were assumed to be in equilibrium. Each measurement within the set of experiments required about 15 min. Equilibrium was established at the highest temperature, the system was cooled stepwise. The measurement method assumes that the system was totally free of leakages. This was verified experimentally by comparing the equilibrium pressures obtained during the heating and the cooling cycles. After a set of experiments was finished, a new set could be carried out by repeating the procedure.

Calculation of Gas-Liquid Solubilities

In this study the gas-liquid solubility of solute 1 in solvent 2 is expressed as a pseudo Henry constant H_{12}^{PS} at

 $P^{\circ} = 1.013$ bar. The following relation holds for both components at gas-liquid equilibrium:

$$f_i^{\rm L} = f_i^{\rm V} \tag{2}$$

Here, the gas-phase fugacity of component i, f_i^V , follows from

$$f_i^{\rm V} = \varphi_i^{\rm V} y_i P \tag{3}$$

where $\varphi_i^{\mathbf{V}}$ = the gas-phase fugacity coefficient of component *i*. In contrast to the gas-phase fugacities, liquid-phase fugacities, $f_i^{\mathbf{L}}$, at constant composition and temperature depend only slightly on the pressure, according to

$$f_{i}^{L}(P) = f_{i}^{L}(P^{\circ}) \exp(\int_{P^{\circ}}^{P} \bar{v}_{i}^{L}(RT)^{-1} \, \mathrm{d}P)$$
(4)

where \bar{v}_i^{L} is the partial molar liquid volume of component *i*. For a dilute solution of solute 1 in solvent 2 the liquid-phase fugacity of the solute is usually given by Henry's law:

$$f_1^L = \gamma_1^* x_1 H_{12}$$
 with $\lim_{x_1 \to 0} (\gamma_1^*) = 1$ (5)

where γ_1^* = the liquid-phase activity coefficient of 1 and H_{12} = the Henry coefficient of solute 1 in solvent 2. Combining eqs 2–5 gives for H_{12}^{PS}

$$H_{12}^{\text{PS}} = \gamma_{12}^{*}(P^{\circ})H_{12}(P^{\circ}) = (\varphi_{1}^{\text{V}}y_{1}P/x_{1})\exp(\int_{P}^{P^{\circ}}\bar{v}_{i}^{\text{L}}(RT)^{-1} dP)$$
(6)

The exponential term is called the Poynting correction (9). $\varphi_1^{\rm V}$ and $\bar{v}_1^{\rm L}$ were calculated with the Peng-Robinson equation of state (10). x_1 and y_1 were obtained from the primary experimental data at equilibrium (P, T, $V_{\rm sys}(T_0)$, $n_1^{\rm T}$, and $n_2^{\rm T}$) via the next set of equations:

1

$$x_1 = \frac{n_1^{\rm L}}{n_1^{\rm L} + n_2^{\rm L}} \tag{7}$$

$$y_1 = 1 - y_2$$
 (8)

$$n_1^{\mathrm{L}} + n_1^{\mathrm{V}} = n_1^{\mathrm{T}} \tag{9}$$

$$n_2^{\rm L} + n_2^{\rm V} = n_2^{\rm T}$$
 (10)

$$V^{\rm L} + V^{\rm V} = V_{\rm sys}(T_0)[1 + \alpha_{\rm SS}(T - T_0)]$$
(11)

$$n_1^{\mathsf{V}} = y_1(PV^{\mathsf{V}}/RTZ^{\mathsf{V}}) \tag{12}$$

$$n_2^{\rm V} = y_2 (PV^{\rm V}/RTZ^{\rm V}) \tag{13}$$

$$y_2 = (x_2 P_2^{\rm s}/{\rm P})({\rm cf})$$
 (14)

$$V^{\rm L} = n_2^{\rm L} v_2^{\,\circ \rm L} + n_2^{\rm L} v_2^{\rm EL} + n_1^{\rm L} \bar{v}_1^{\rm L} \tag{15}$$

$$v_2^{\circ L} = [\varrho_2^L(P,T)/M_2]^{-1}$$
 (16)

$$v_2^{\rm EL} = \bar{v}_2^{\rm L}|_{\rm PR} - v_2^{\circ \rm L}|_{\rm PR} \tag{17}$$

$$\bar{v}_1^{\mathrm{L}} = \bar{v}_1^{\mathrm{L}}|_{\mathrm{PR}} \tag{18}$$

$$Z^{\mathbf{V}} = f(P, T, y_1, y_2) \tag{19}$$

Table 2. Relevant Physical Properties of the Chemicals Used in This Study: Molecular Weights (M), Boiling Points (T_b), Critical Properties (P_c , T_c , Z_c), and Acentric Factors (ω) (Values Obtained from Daubert and Danner (13) If Not Noted Otherwise)

component	M/(kg kmol ⁺¹)	$T_{\rm b}/{ m K}$	$P_{\rm c}/{\rm bar}$	$T_{\rm c}/{ m K}$	$Z_{ m c}$	ω
H ₂	2.02	20.38	12.83	33.20	0.305	-0.2200
CÔ	28.01	81.70	34.54	132.92	0.295	0.0663
CO_2	44.01	194.80	72.87	304.19	0.274	0.2276
C_2H_6	30.07	184.55	48.17	305.42	0.284	0.0990
C_3H_8	44.10	231.11	41.94	369.82	0.280	0.1517
$C_{5}H_{12}$	72.15	309.22	33.26	469.65	0.269	0.2486
$C_{6}H_{14}$	86.18	341.88	29.73	507.43	0.264	0.3047
CH₃OH	32.04	337.85	79.92	512.58	0.224	0.5656
C_2H_5OH	46.07	351.44	63.02	516.25	0.248	0.6371
1-C ₃ H ₇ OH	60.10	370.35	51.04	536.71	0.253	0.6279
1-C₄H ₉ OH	74.12	390.81	43.56	562.93	0.259	0.5945
$1-C_5H_{11}OH$	88.15	410.95	38.30	586.15	0.260	0.5938
$1-C_6H_{13}OH$	102.18	430.15	34.65	611.35	0.263	0.5803
H_2O	18.02	373.15	218.07	647.29	0.233	0.3442
$C_8H_{18}O_5$	194.23	581.00	25.57	722.00	0.243	1.5783
$C_{10}H_{14}$	178.23	613.45	28.63	869.25	0.222	0.4858
$C_{16}H_{34}$	226.45	560.00	14.01	720.60	0.228	0.7471
$1-C_{16}H_{33}OH$	242.45	617.00^{a}	14.92^{b}	764.18^{b}	0.222^{b}	1.2308°
$C_{28}H_{58}$	394.78	704.60 ^a	8.81^{b}	866.20 ^b	0.199^{b}	0.8590°

 a Estimated with the method of Weast et al. (14). b Estimated with the method of Lydersen (15). c Estimated with the Lee–Kesler method (16).

$$\mathrm{cf} = \left(\frac{\varphi_2^{\circ^{\mathrm{V}}}(P_2^{\mathrm{s}}, T)}{\varphi_2^{\mathrm{V}}}\right) \tag{20}$$

where V^{L} = the volume of liquid in the vessel, V^{V} = the volume of gas in the vessel, α_{SS} = the cubic thermal expansion coefficient of stainless steel, i.e., $5.2 \times 10^{-5} \, \mathrm{K}^{-1}$ (12), Z^{V} = the compressibility factor of the gas phase, n^{L} = the number of moles in the liquid phase, n^{V} = the number of moles in the gas phase, P_2^s = the saturated vapor pressure of the pure solvent, cf = the correction factor for nonideal behavior of the gas phase concerning the vapor pressure of the solvent, $v^{\circ L}$ = the molar pure liquid volume, v_2^{EL} = the molar liquid excess volume of the solvent, ϱ_2^{L} (P,T) = the pure liquid density of the solvent at P and T, M_2 = the molar mass of the solvent, $|_{PR}$ = calculated with the Peng-Robinson equation of state, $\varphi_2^{\circ V}(P_2^s,T) =$ the gas-phase fugacity coefficient of the pure solvent at P_2^s and T, and 1 and 2 refer to the solute and solvent, respectively. In Table 2 the relevant physical properties of the pure components are presented. The liquid density of the solvent at a standard pressure of $P^{\circ} = 1$ bar, ϱ_2^{\perp} (P°,T) , was calculated for hexadecane, tetraethylene glycol, and phenanthrene with an empirical equation from Daubert and Danner (13) and for 1-hexadecanol and octacosane with the method as proposed by Spencer and Danner (17). The liquid density of the solvent at increased pressure, $\varrho_2^{L}(P,T)$, was calculated via (18)

$$\varrho_2^{\rm L}(P,T) = \varrho_2^{\rm L}(P^\circ,T) \left(1 + \frac{9Z_{\rm c,2}N(P-P^\circ)}{P_{\rm c,2}}\right)^{1/9} \quad (21)$$

with $N = (1 - 0.89\omega_2^{1/2}) \exp(6.9547 - 76.2853T_{r,2} + 191.306T_{r,2}^2 - 203.5472T_{r,2}^3 + 82.76T_{r,2}^4)$. Here, Z_c = the critical compressibility factor, P_c = the critical pressure, ω = the acentric factor, and T_r = the reduced temperature. Although eq 21 is for apolar or weakly polar liquids, it could also be used for 1-hexadecanol and tetraethylene glycol without being a serious additional error source (see also below) because the pressure corrections were usually small. For hexadecane, tetraethylene glycol, and phenanthrene the vapor pressure was calculated via an empirical equa-

tion from Daubert and Danner (13) and for 1-hexadecanol and octacosane via a method proposed by Riedel (19). The values of Z^{v} , $\varphi_{2}^{\circ v}$, φ_{2}^{v} , and the molar liquid volumes $v_{2}^{\circ L}|_{PR}$, $\bar{v}_{1}^{L}|_{PR}$, and $\bar{v}_{2}^{L}|_{PR}$ were all calculated with the Peng-Robinson equation of state, the latter two numerically by using a finite difference technique with Δn_{j}^{L} equal to 1% of n_{j}^{L} . For example, for $v_{1}^{L}|_{PR}$

$$v_1^{\rm L}|_{\rm PR} = \frac{(n_1^{\rm L} + \Delta n_1^{\rm L} + n_2^{\rm L})v^{\rm L'} - (n_1^{\rm L} + n_2^{\rm L})v^{\rm L}}{\Delta n_1^{\rm L}} \qquad (22)$$

Here, $v^{L'}$ and v^{L} are the liquid-phase molar volumes at compositions $(n_1^{L} + \Delta n_1^{L}, n_2^{L})$ and (n_1^{L}, n_2^{L}) , respectively. In eqs 6–20, the Peng–Robinson equation of state was used with zero binary interaction coefficients because the values available for these coefficients (11) were not suitable to predict accurately either gas-phase fugacity coefficients or liquid densities. It was checked that using zero binary interaction coefficients did not affect the accuracy of the results. The set of nonlinear equations (7–20) was numerically solved by successively substituting x_1 . The updating equation for x_1 was taken as follows:

$$x_1^{n+1} = x_1^n + \beta(F(x_1^n) - x_1^n)$$
(23)

Here, $F(x_1^n)$ represents the new computed value for x_1 , with the iterative scheme set up in the form $x_1^{n+1} = F(x_1^n)$. β is a relaxation factor to obtain convergency $(0 \le \beta \le 1)$. The starting value for y_1 was taken as 1, and that for x_1 followed by setting $y_1 = 1$, $Z^V = 1$, cf = 1, $v_2^{EL} = 0$, and $\bar{v}_1^L = 0$. The value of the relaxation factor (between 0 and 1) and the number of iterative steps required to match the convergency criterion, i.e., $|x_1^{n+1} - x_1^n| \le 10^{-4}x_1^n$, depended particularly on the nonideality of both the liquid and gas phases.

Error in x_1 and H_{12}^{PS} . The maximal and average errors in H_{12}^{PS} , ERR_{MAX}^{H} , and ERR_{AV}^{H} , respectively, were obtained from the maximal absolute errors of the various error sources as listed in Table 3, via (7)

$$\mathrm{ERR}_{\mathrm{MAX}}^{H} = 100 \sum_{k=1}^{N_{\mathrm{err}}} \frac{\partial H_{12}^{\mathrm{PS}}}{\partial v_{k}} \frac{(\Delta v_{k}^{\mathrm{sys,rp}} + \Delta v_{k}^{\mathrm{lof}})}{H_{12}^{\mathrm{PS}}} \qquad (24)$$

$$\mathrm{ERR}_{\mathrm{AV}}^{H} = 100 \left(\sum_{k=1}^{N_{\mathrm{erf}}} \left(\frac{\partial H_{12}^{\mathrm{PS}}}{\partial v_{k}} \frac{(\Delta v_{k}^{\mathrm{sys,rp}} + \Delta v_{k}^{\mathrm{lof}})}{H_{12}^{\mathrm{PS}}} \right)^{2} \right)^{1/2} \quad (25)$$

where $N_{\rm err}$ = the total number of error-contributing variables, v = an error-contributing variable, for example, W_1 , W_2 , etc. (see Table 3), and Δv = the absolute error in variable v, with sys,rp and lof indicating errors due to systematic and reproducibility effects and due to lack of fit, respectively. For the errors in x_1 , ERR^{*}_{MAX} and ERR^{*}_{AV}, the same equations hold with $H_{12}^{\rm PS}$ replaced by x_1 . For those variables in eqs 24 and 25 which depend on P, T, n_1^T , and/or n_2^T (for example, y_1) the value of $\Delta v_k^{\rm sys/rp}$ is estimated via

$$\Delta v_k^{\text{sys,rp}} = \frac{\partial v_k}{\partial \mathbf{P}} \Delta \mathbf{P} + \frac{\partial v_k}{\partial \mathbf{T}} \Delta \mathbf{T} + \frac{\partial v_k}{\partial n_1^{\text{T}}} \Delta n_1^{\text{T}} + \frac{\partial v_k}{\partial n_2^{\text{T}}} \Delta n_2^{\text{T}} \quad (26)$$

All partial derivatives in eqs 24-26 were calculated numerically with a finite difference technique by varying v_k , P, T, n_1^T , or n_2^T by 1%.

Results and Discussion

Gas-Liquid Solubilities. Gas-liquid solubilities of 60 binaries were measured as a function of temperature. For

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Table 3. Estimated Absolute Values of the VariousErrors

error source	systematical error and reproducibility	lack of fit	units
	0.01^{a} 0.0001^{a} 0.5^{a} 0.15^{b} 0.015^{b} 0.3^{b} g g g g g g g g	$\begin{array}{c} 0.1 P_2^{\mathrm{S}f} \\ 0.2 v_1^{\mathrm{L}f} \\ 0.2 v_2^{\mathrm{E}\mathrm{L}f} \\ 0.015 Z^{\mathrm{V}d} \\ 0.005 v_2^{\mathrm{o}\mathrm{L}e} \\ 0.005 \varphi_1^{\mathrm{V}d} \\ 0.002 \varphi_1^{\mathrm{V}d} \end{array}$	g g bar K bar m ³ mol ⁻¹ m ³ mol ⁻¹ m ³ mol ⁻¹
	g	$0.010 arphi_1^{\mathrm{V}\ d}$	
	g	$0.015 arphi_1^{\mathrm{V}\ d}$	

^a Estimated from the inaccuracy of the balance (for a differential mass, twice the inaccuracy per reading). ^b Estimated from the results of repeated measurements and the inaccuracy of the calibration equipment. ^c Estimated from the standard deviation of repeated measurements. ^d Estimated by Graaf et al. (7). ^e Estimated from the difference between predicted and experimental data from Spencer and Danner (17). ^f Estimated from the inaccuracies of pure component vapor pressures (5%) and liquid molar volumes (10%) as predicted from the Peng-Robinson equation of state (10). ^g These error sources show neither systematic nor reproducibility errors directly. However, the corresponding values depend on P, T, and/or composition. So, indirectly errors in these parameters are present as calculated from eq 26.



Figure 3. Solubility of hydrogen in various solvents as a function of the temperature: (∇) tetraethylene glycol, (\diamond) phenanthrene, (\bigcirc) hexadecane, (\triangle) 1-hexadecanol, (\Box) octacosane, (-) Peng-Robinson equation of state with optimization of two binary interaction parameters; see Breman et al. (11).

the results see the Appendix, Tables A1-A60. As can be seen in the Appendix, both y_2 and the Poynting correction (Pntr) were always small. The highest values are 0.19 and 1.203, respectively. Further, even for the binary system with the lowest gas-liquid solubility, the relative fraction of dissolved solute was significant: hydrogen-tetraethylene glycol at T = 454.9 K, $n_1^L/n_1^T = 0.16$. Calculations with the Peng-Robinson equation of state, using two optimized binary interaction parameters (11), indicate that γ_1^* in eq 5 always deviates less than 10% from 1. As a result, the pseudo Henry coefficient H_{12}^{PS} (see eq 6) deviates less than 10% from the real Henry coefficient H_{12} .



Figure 4. Solubility of carbon monoxide in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 5. Solubility of carbon dioxide in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 6. Solubility of water in various solvents as a function of the temperature. See Figure 3 for symbols.

 H_{12}^{PS} is shown as a function of temperature for each solute in the various solvents in Figures 3–16. The solid line is predicted from the Peng-Robinson equation of state after optimization of two binary interaction parameters (11). For the alcohols, the paraffins, and water the gasliquid solubilities always decrease with increasing temperature, implying an exothermic dissolving process. In contrast, the small nonpolar solute molecules carbon monoxide and hydrogen dissolve endothermically or just weakly exothermically. This indicates relatively weak



Figure 7. Solubility of ethane in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 8. Solubility of propane in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 9. Solubility of pentane in various solvents as a function of the temperature. See Figure 3 for symbols.

intermolecular forces between these small molecules and the solvent molecules. For the binary system carbon dioxide-tetraethylene glycol a similar result is observed at high temperatures; see Figure 5. Although water is also a small molecule, obviously its strong polarity guarantees an exothermic dissolving process in all solvents over the whole temperature range.

$$m_{12} = \frac{c_1^{\rm L}}{c_1^{\rm V}} = \frac{x_1 v^{\rm V}}{y_1 v^{\rm L}} \tag{27}$$



Figure 10. Solubility of hexane in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 11. Solubility of methanol in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 12. Solubility of ethanol in various solvents as a function of the temperature. See Figure 3 for symbols.

Table 4 gives an overview of all experimental H_{12}^{PS} and m_{12} values at 498 K. Here, the gas-liquid solubility m_{12} is defined by

The molar liquid and gas volumes in eq 27 were calculated as discussed above. The tendencies observed at 498 K are rather typical for the whole temperature range. Relative to the corresponding paraffins, the gas-liquid solubilities of the alcohols are always higher. As expected, this relative difference is much larger for a polar solvent such as 1-hexadecanol than for an apolar solvent such as octacosane. For water and the alcohols, tetraethylene glycol



Figure 13. Solubility of 1-propanol in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 14. Solubility of 1-butanol in various solvents as a function of the temperature. See Figure 3 for symbols.



Figure 15. Solubility of 1-pentanol in various solvents as a function of the temperature. See Figure 3 for symbols.

clearly is the best solvent. Depending on the carbon number of the solute, either 1-hexadecanol [alcohols $(n \le 4)$ and water] or phenanthrene [alcohols (n > 4)] is the second best solvent, whereas octacosane [alcohols $(n \le 4)$] and hexadecane [water and alcohols (n > 4)] are the poorest solvents. For hydrogen, carbon monoxide, carbon dioxide, and the paraffins, hexadecane is the best solvent (measurements in three solvents only) and phenanthrene (carbon dioxide and carbon monoxide) or tetraethylene glycol (hydrogen) is the poorest solvent. The gas-liquid solubilities of carbon dioxide appear to be much more sensitive to



Figure 16. Solubility of 1-hexanol in various solvents as a function of the temperature. See Figure 3 for symbols.

Table 4. Pseudo Henry Constants H_{12}^{PS} (bar) and Solubility Constants m_{12} (Dimensionless) at T = 498 K Obtained via Linear Interpolation from the Appendix

				solvent		
solute		$\mathrm{C_8H_{18}O_5}$	$C_{10}H_{14}$	$C_{16}H_{34}$	1-C ₁₆ H ₃₃ OH	$C_{28}H_{58}$
H ₂	H_{12}^{PS}	2139.3	1862.2	576.6	667.0	523.8
	m_{12}	0.092	0.122	0.197	0.178	0.137
CO	H_{12}^{PS}	1738.8	2551.8	441.7	552.1	329.8
	m_{12}	0.113	0.089	0.257	0.214	0.217
CO_2	H_{12}^{PS}	376.7	648.7	191.4	216.6	187.3
	m_{12}	0.520	0.351	0.592	0.547	0.383
C_2H_6	H_{12}^{PS}			120.4	151.7	86.3
	m_{12}			0.916	0.781	0.831
C_3H_8	H_{12}^{PS}			82.1	104.5	51.5
	$m_{12}^{}$			1.323	1.133	1.392
$C_{5}H_{12}$	H_{12}^{PS}			26.1	31.8	21.9
	$m_{12}^{}$			4.344	3.731	3.268
C_6H_{14}	H_{12}^{PS}			17.2	20.0	12.1
	m_{12}			6.578	5.917	5.917
CH ₃ OH	H_{12}^{PS}	29.1	95.7	68.4	40.2	49.5
	m_{12}	6.757	2.387	1.661	2.950	1.449
C_2H_5OH	$H_{12}^{ m PS}$	26.9	69.9	47.3	30.1	36.0
	$m_{12}^{}$	7.299	3.268	2.404	3.937	1.992
$1-C_3H_7OH$	H_{12}^{PS}	16.6	38.4	30.0	18.9	20.2
	m_{12}	11.905	5.952	3.788	6.289	3.559
$1-C_4H_9OH$	H_{12}^{PS}	14.5	21.5	18.7	12.7	12.7
	$m_{12}^{}$	13.513	10.638	6.098	9.346	5.650
$1-C_5H_{11}OH$	H_{12}^{PS}	10.8	17.2	15.8	11.3	8. 9
	m_{12}	18.182	13.333	7.194	10.526	8.064
$1-C_6H_{13}OH$	H_{12}^{PS}			11.7	6.9	5.5
	m_{12}			9.709	17.241	13.158
H_2O	H_{12}^{PS}	18.3	122.1	105.6	59.5	55.0
	m_{12}	10.753	1.869	1.075	1.992	1.304

the chemical nature of the solvent than those of carbon monoxide and hydrogen. This can be understood from the high polarizability of carbon dioxide. The gas-liquid solubilities of carbon monoxide, carbon dioxide, and hydrogen in hexadecane are comparable to those in 1-hexadecanol, indicating a minor influence of the solvent hydroxide group of the latter solvent for these solutes. The gas-liquid solubilities of both the alcohols and water are significantly higher in 1-hexadecanol than in hexadecane whereas the paraffins show the opposite behavior, indicating a significant influence of the solvent hydroxide group of 1-hexadecanol for these solutes. The gas-liquid solubilities in hexadecane and octacosane can differ substantially despite their similar chemical nature. This indicates a

solute	solvent	T/K	$H_{12}^{ m PS,LIT}/ m bar$	H_{12}^{PS} /bar	$100(\mathbf{RR})^d$	ref
$\overline{\mathrm{CO}_2}$	$C_{10}H_{14}$	382	$400.0^{a,b}$	420.8°	4.9	Barrick et al. (22)
$\rm CO_2$	$C_{10}H_{14}$	423	$466.0^{a,b}$	493.6	5.6	Barrick et al. (22)
H_2	$C_{16}H_{34}$	353	902.0 ^a	901.5	0.1	Graaf et al. (7)
H_2	$\mathrm{C_{16}H_{34}}$	300	1111.0	966.0	15.0	Cukor and Prausnitz (6)
H_2	$C_{16}H_{34}$	425	681.0	729.9	6.7	Cukor and Prausnitz (16)
H_2	$C_{16}H_{34}$	475	567.0	621.1	8.7	Cukor and Prausnitz (6)
CO	$C_{16}H_{34}$	298	567.0ª	569.3 ^c	0.4	Graaf et al. (7)
CO	$C_{16}H_{34}$	353	517.0^{a}	59 0.8	12.5	Graaf et al. (7)
CO	$C_{16}H_{34}$	300	538.0	566.7°	5.1	Tremper and Prausnitz (21)
CO	$C_{16}H_{34}$	425	461.0	521.9	11.7	Temper and Prausnitz (21)
CO	$C_{16}H_{34}$	475	419.0	466.4	10.2	Temper and Prausnitz (21)
CO	$\mathrm{C_{16}H_{34}}$	298	570.0	569.3°	0.1	Lin and Parcher (20)
CO	$C_{16}H_{34}$	328	543.0	603.5	10.0	Lin and Parcher (20)
$\rm CO_2$	$C_{16}H_{34}$	298	74.0	66.0 ^c	12.2	Graaf et al. (7)
CO_2	$C_{16}H_{34}$	353	115.0	116.4	1.2	Graaf et al. (7)
$\rm CO_2$	$C_{16}H_{34}$	300	74.0	67.3^{c}	10.0	Tremper and Prausnitz (21)
CO_2	$C_{16}H_{34}$	425	157.0	164.9	4.8	Temper and Prausnitz (21)
CO_2	$C_{16}H_{34}$	475	176.0	185.6	5.2	Temper and Prausnitz (21)
$\rm CO_2$	$C_{16}H_{34}$	298	71.0	66.0°	7.6	Chai and Paulaitis (23)
$\rm CO_2$	$C_{16}H_{34}$	330	95.0	98.0	3.1	Chai and Paulaitis (23)
CO_2	$C_{16}H_{34}$	298	73.0	66.0	10.7	Lin and Parcher (20)
$\rm CO_2$	$C_{16}H_{34}$	328	92.0	96.3	4.5	Lin and Parcher (20)
C_5H_{12}	$C_{16}H_{34}$	320	$1.3^{a,b}$	1.2°	5.0	Donohue et al. (24)
H_2	$\mathrm{C}_{28}\mathrm{H}_{58}$	528	$406.0^{a,b}$	488.2 ^c	16.0	Miller and Ekstrom (25)
CO	$\mathrm{C}_{28}\mathrm{H}_{58}$	528	$352.6^{a,b}$	307.0°	12.1	Miller and Ekstrom (25)
$\rm CO_2$	$C_{28}H_{58}$	353	82.0	92.4°	11.2	Lin and Parcher (20)
$\rm CO_2$	$\mathrm{C}_{28}\mathrm{H}_{58}$	393	101.0	115.9 ^c	12.8	Lin and Parcher (20)
C_2H_6	$\mathrm{C}_{28}\mathrm{H}_{58}$	393	54.0	52.8°	2.3	Lin and Parcher (20)
C_3H_8	$C_{28}H_{58}$	353	15.4	14.2°	8.8	Lin and Parcher (20)
C_3H_8	$\mathrm{C}_{28}\mathrm{H}_{58}$	393	24.7	22.3°	10.6	Lin and Parcher (20)

 Table 5.
 Comparison with Data Available from the Literature

^a Corrected to P° bar via eq 4. If not noted, no correction was carried out because the exact experimental pressure was not given. ^b Calculated from liquid composition and equilibrium pressure via eq 6 with y_1 taken equal to 1. ^c Obtained via the Peng-Robinson equation of state after optimization of two binary interaction parameters; see Breman et al. (11). If not noted, obtained via linear interpolation from the Appendix. ^d Defined by $RR = |1 - H_{12}^{PS,LIT}/H_{12}^{PS}|$.

significant influence of the size and/or shape of the solvent molecule on the gas-liquid solubilities. Especially for the small apolar solute molecules hydrogen, carbon monoxide, and carbon dioxide, the gas-liquid solubility is higher in hexadecane than in octacosane, whereas for the other solutes this difference is relatively smaller; see Table 4.

Comparison with Literature Data. Not many gasliquid solubility data are available for the investigated binary systems. For all the binaries with either an alcohol or water as the solute and/or tetraethylene glycol, 1-hexadecanol, and phenanthrene (except if carbon dioxide is the solute) as the solvent, no comparable measurements were found in the literature. For the other binary systems some results are available. However, these results were nearly always obtained at pressures below or at 1.013 bar, and for a few temperatures only. These limitations usually originate from the experimental methods applied (20, 21). The present set of results therefore substantially extends the gas-liquid solubility data bank. It is especially relevant to gas-slurry processes for methanol (-higher alcohol) and hydrocarbon production from synthesis gas. In Table 5 the limited literature results available are compared to our corresponding experimental data. It should be noted that the reported literature values of the pseudo Henry coefficient, $H_{12}^{PS,LIT}$, were generally obtained at another composition of the liquid phase. However, calculations with the Peng-Robinson equation of state suggest that H_{12}^{PS} deviates less than 5% from H_{12} for the binary systems listed in Table 5, allowing a direct comparison between the pseudo Henry coefficients from the literature and this study to be made. As appears from Tables 5 and 6, the agreement between the gas-liquid solubilities from the literature and those from this study is satisfactory, with deviations always within the calculated average experimental errors.

Experimental Errors. For the minimal, maximal, and average calculated values of the average error in x_1 $(\text{ERR}_{\text{AV}}^x)$ and H_{12}^{PS} $(\text{ERR}_{\text{AV}}^H)$ and the maximal values of the maximal error in x_1 $(\text{ERR}_{\text{MAX}}^x)$ and H_{12}^{PS} $(\text{ERR}_{\text{MAX}}^H)$, see Table 6. The maximal values of $\text{ERR}_{\text{MAX}}^x$ and $\text{ERR}_{\text{MAX}}^H$ are higher than the maximal values of ERR_{AV}^{x} and ERR_{AV}^{H} because the first two were calculated from a worst case approach assuming all error sources contributing maximally in the same direction to the overall error, which is very unlikely to occur in practice. The values of ERR_{AV}^{x} and ERR^{H}_{AV} are still overestimated because these are also calculated assuming all the error sources contributing in the same direction to the overall error though not with their maximal quantities but rather with a kind of average quantity, also still unlikely to occur in practice. A high gas-liquid solubility and a relatively large amount of solvent are favorable to obtain accurate results. The first effect is seen from comparing, for example, the errors in the binary systems containing carbon monoxide or hydrogen and the errors in the binary systems containing alcohols. The second effect follows from comparing the errors in binary systems containing hexadecane (± 2 mol of solvent) and the binary systems containing octacosane $(\pm 0.4 \text{ mol of solvent})$. As far as possible, we used relatively large amounts of solute and solvent.

In Table 7 the relative individual contributions of the several error sources to ERR_{MAX}^x and ERR_{MAX}^H are shown for some binary systems. Neither for low (represented by carbon monoxide and hydrogen) nor for high gas-liquid solubilities (represented by ethanol and 1-pentanol) can dominating error sources be identified for ERR_{MAX}^x . Therefore, further improvement of the experimental accuracy in the measurement of temperature, pressure, system volume, or total amounts of solute and solvent will

Table 6.	Minimal, Maxima	il, and Average	Values of t	he Average	Relative	Error in x_1	(ERR_{AV}^{x}) and H_{12}^{PS}	(ERR_{AV}^{H}) and
Maximal	Values of the Max	cimal Relative I	Error in x_1 (ERR ^x _{MAX}) and	d H_{12}^{PS} (ER	\mathbb{R}_{MAX}^H) for all	Binaries	

			\mathbf{ERR}_{AV}^{x}			$\mathbf{ERR}_{\mathbf{AV}}^{\mathbf{H}}$		ERR	ERRH
solute	solvent	min	max	av	min	max	av	max	max
H_2	$C_8H_{18}O_5$	13.18	62.17	27.66	17.96	93.47	40.09	93.97	94.08
CŌ	$C_8H_{18}O_5$	8.85	43.75	21.06	11.71	68.84	30.97	67.59	70.37
CO_2	$C_8H_{18}O_5$	2.15	4.90	4.13	3.49	6.24	5.45	5.94	7.77
$CH_{3}OH$	$C_8H_{18}O_5$	0.21	1.23	0.56	1.67	2.19	1.77	1.45	3.66
C_2H_5OH	$C_8H_{18}O_5$	0.18	0.88	0.48	1.68	1.93	1.77	1.06	3.20
$1-C_{3}H_{7}OH$	$C_8H_{18}O_5$	0.13	0.66	0.35	1.71	2.46	1.85	0.83	3.70
$1-C_4H_9OH$	$C_8H_{18}O_5$	0.16	0.59	0.34	1.72	2.04	1.80	0.75	3.22
$1-C_5H_{11}OH$	$C_8H_{18}O_5$	0.15	0.47	0.26	1.82	2.48	2.02	0.64	3.85
H_2O	$C_8H_{18}O_5$	0.18	0.77	0.41	1.66	1.87	1.74	0.97	3.13
H_2	$C_{10}H_{14}$	14.80	20.20	17.57	21.38	30.43	25.91	30.73	31.16
00	$C_{10}H_{14}$	14.49	21.04	17.16	20.21	30.70	24.51	30.92	31.95
CO_2	$C_{10}H_{14}$	5.80	6.74	6.45	7.94	8.61	8.45	8.38	10.14
CH ₃ OH	$C_{10}H_{14}$	0.55	1.30	0.95	1.79	2.31	2.00	1.67	3.77
C_2H_7OH	$C_{10}H_{14}$	0.41	1.13	0.75	1.70	2.11	1.00	1.37	0.0Z 2.07
$1-C_3\Pi_7$ OH	$C_{10} H_{14}$	0.21	0.74	0.40	1.74	1.99	1.01	0.91	3.27
	$C_{10}\Pi_{14}$	0.10	0.00	0.30	1.70	2.10	1.00	0.71	3.50
1-05n110n		0.18	1.90	1 36	1.80	2.17	1.34	0.02	1 34
1120 H	C_{10}	15.03	29.49	20.53	18 50	41.98	2.52	42 59	42.69
	$C_{16} H_{04}$	11.68	18 37	14 48	13.00	24.28	17.69	24.03	25 39
CO.	CicHa	3 59	6.01	516	5.02	7 04	6 45	6.87	8.61
CoHe	$C_{16}H_{04}$	1.69	4 56	3 33	3.60	5.60	4 62	5.33	6.60
C ₂ H ₆	$C_{16}H_{24}$	0.91	272	2 11	2 70	4.20	3.13	3.20	4.81
C _z H ₁₀	$C_{16}H_{24}$	0.27	0.90	0.56	1.80	2.09	1.87	1.09	3.32
CeH14	$C_{16}H_{34}$	0.30	0.60	0.43	1.86	2.16	1.94	0.80	3.61
CH ₃ OH	C16H34	0.44	1.37	1.01	1.99	2.33	2.16	1.76	3.78
C ₂ H ₅ OH	$C_{16}H_{34}$	0.35	1.11	0.69	2.01	2.81	2.17	1.52	4.45
1-C ₃ H ₇ OH	$C_{16}H_{34}$	0.21	0.80	0.45	1.94	4.67	2.50	1.11	6.34
1-C₄H ₉ OH	$C_{16}H_{34}$	0.25	0.63	0.39	1.86	2.45	2.08	0.84	3.92
$1-C_5H_{11}OH$	$C_{16}H_{34}$	0.22	0.53	0.29	2.13	17.75	6.57	0.83	19.63
$1-C_6H_{13}OH$	$C_{16}H_{34}$	0.32	0.51	0.36	2.76	34.86	11.82	0.88	36.97
H_2O	$C_{16}H_{34}$	1.09	2.19	1.69	2.19	3.20	2.72	2.83	4.78
H_2	$1 - C_{16}H_{33}OH$	17.42	22.88	20.23	23.91	33.31	28.66	33.77	34.07
CO	$1 - C_{16}H_{33}OH$	13.91	17.82	15.77	17.14	23.71	20.20	23.86	24.83
CO_2	$1 - C_{16}H_{33}OH$	5.78	6.89	6.41	7.90	8.63	8.36	8.48	10.28
C_2H_6	$1 - C_{16}H_{33}OH$	3.82	5.04	4.49	5.68	6.64	6.24	6.70	9.22
$C_{3}H_{8}$	$1-C_{16}H_{33}OH$	2.30	3.11	2.67	5.53	6.29	5.70	4.53	8.45
C_5H_{12}	$1 - C_{16}H_{33}OH$	0.28	0.73	0.45	2.19	5.76	3.06	1.10	7.58
C_6H_{14}	$1 - C_{16}H_{33}OH$	0.24	0.53	0.32	2.59	11.50	4.99	0.84	13.30
	$1-C_{16}H_{33}OH$	0.23	1.23	0.65	1.97	4.80	2.43	1.00	0.00
		0.20	0.98	0.50	1.90	1.21	2.00	1.04	9.01 7.90
1-C3H7OH	1 C. H. OH	0.20	0.00	0.42	2.40	32.40	0.21	0.79	24 02
1-C-HOH	1-C16H33OH	0.22	0.30	0.28	2.01	10.06	3.80 4.78	0.75	12.24
1-C.H.OH	1-C16H330H	0.20	0.38	0.28	4 45	18.17	8.07	0.66	20.97
H ₀ O	1-C16H33OH	0.24	1.63	0.85	2.14	4 64	2.61	2.28	6.44
	CooHea	57.87	69.52	65.76	77.10	106.52	94.51	101.70	107.48
cô	C28H58	36.08	45.44	41.12	42.59	67.24	55.58	62.61	68.69
CO_2	$C_{28}H_{58}$	20.31	25.31	22.53	26.81	38.85	32.70	35.58	41.02
C_2H_6	$C_{28}H_{58}$	10.01	10.73	10.32	12.73	15.23	13.92	14.04	17.72
C_3H_8	$C_{28}H_{58}$	7.50	9.76	8.49	12.41	15. 91	13.91	15.67	20.01
C_5H_{12}	$C_{28}H_{58}$	1.48	3.06	2.21	3.36	4.99	4.03	4.85	7.33
C_6H_{14}	$C_{28}H_{58}$	0.67	1.79	1.10	2.88	5.58	3.41	2.90	7.91
CH₃OH	$C_{28}H_{58}$	5.22	6.20	5.61	8.29	9.64	8.80	9.65	12.24
C_2H_5OH	$C_{28}H_{58}$	2.06	4.52	3.21	3.37	6.28	4.71	6.18	8.21
$1-C_3H_7OH$	$C_{28}H_{58}$	0.57	2.73	1.57	2.40	4.08	2.99	3.84	5.94
$1-C_4H_9OH$	$C_{28}H_{58}$	0.73	1.77	1.20	2.54	3.11	2.71	2.70	5.01
$1-C_5H_{11}OH$	$C_{28}H_{58}$	0.64	1.35	0.95	2.56	3.11	2.70	2.17	5.16
$1-C_6H_{13}OH$	$C_{28}H_{58}$	0.56	0.88	0.66	2.68	9.46	4.65	1.55	11.78
H_2O	$C_{28}H_{58}$	1.58	7.61	5.04	3.36	11.45	7.87	11.57	13.78

reduce the overall value of $\text{ERR}_{\text{MAX}}^{\text{x}}$ only partially. The total error is relatively strongly influenced by the assumed lack of fit in the calculation of the liquid-phase molar volumes v_1^{L} , v_2^{EL} , and $v_2^{\circ \text{L}}$ and the gas-phase compressibility factor Z^{V} if the lack of fit errors are those of Table 3. Then a further improvement in the accuracy of x_1 and H_{12}^{PS} requires more accurate methods to predict the gas and liquid densities. In contrast, the influence of the inaccuracies in P_2^{S} is negligible. For $\text{ERR}_{\text{MAX}}^{H}$ the same holds as for $\text{ERR}_{\text{MAX}}^{\text{x}}$ unless ethanol or 1-pentanol is the solute. In the latter case the experimental inaccuracy of the pressure measurement and the assumed lack of fit in

the calculation of the gas-phase fugacity coefficient of the solute are the dominating error sources. Especially at low system pressures, where the relative error in the measured pressure is relatively high, as for the 1-pentanol-hexade-cane binary, a further improvement of the accuracy in the pressure measurement will result in a lower $\text{ERR}_{\text{MAX}}^H$.

Conclusions

A large set of new gas-liquid solubility data, potentially relevant for synthesis gas conversion into alcohols and hydrocarbons via gas-slurry processes, has been obtained at the high pressures and temperatures relevant for these

Table 7.	Individual Contributions of the Various Error Sources to the Total Error in x_1 and H_{12}^{PS} for Four Bina	ry
Systems	(Averaged over All Data of a Series of Experiments of the Corresponding Binary System)	-

error	$H_2 - C_{16}H_{34}$		$CO-C_{16}H_{34}$		C_2H_5OH	$\mathrm{C_{2}H_{5}OH-C_{16}H_{34}}$		$1 - C_5 H_{11} OH - C_{16} H_{34}$	
source	ERR ^x	ERR ^H	ERR ^x	ERR ^H	ERR ^x	ERR ^H	ERR ^x	\mathbf{ERR}^{H}	
W ₁	13.26	13.00	1.18	1.12	1.75	0.48	1.81	0.10	
W_2	3.22	3.16	3.52	3.35	13.75	3.85	26.21	1.57	
Р	4.15	5.23	4.97	6.85	11.80	32.44	30.02	75.93	
T	2.11	2.07	2.16	2.06	2.04	0.70	1.27	0.22	
$P_2^{\rm S}$	0.00	0.01	0.01	0.01	0.87	1.83	1.83	1.81	
$\bar{v}_1^{\hat{L}}$	7.63	7.47	11.30	10.72	9.46	2.66	6.82	0.40	
$v_2^{\pm L}$	28.37	27.77	34.65	32.17	21.36	5.98	9.81	0.58	
$\tilde{V}_{svs}(T_0)$	8.18	8.01	8.40	8.01	7.41	2.07	4.08	0.23	
Z	19.12	18.73	19.36	18.47	19.21	5.42	12.22	0.73	
v2°L	13.90	13.62	14.41	13.02	12.29	3.45	6.02	0.35	
$\varphi_1^{\overline{V}}$	0.00	0.87	0.00	2.66	0.00	41.07	0.00	18.02	

processes. The experimental arrangement is particularly suitable to obtain gas-liquid solubilities over wide temperature ranges within a relatively short period of time. The accuracy of the results is reasonable as follows from both calculations and a comparison with the few literature results available.

In general, the gas-liquid solubilities decrease with temperature except for some binary systems with carbon monoxide or hydrogen as the solute.

For both water and the alcohols, the strongly polar tetraethylene glycol is the best solvent and the apolar solvents hexadecane and octacosane are the poorest solvents. In contrast, tetraethylene glycol is the poorest solvent for hydrogen and the poorest but one for carbon monoxide, whereas hexadecane and octacosane are relatively good solvents for these solutes.

Acknowledgment

The authors appreciate the technical assistance of O. Staal and P. Dijkema.

Notation

с	concentration, mol m ⁻³
$\mathrm{ERR}^{H}_{\mathrm{AV}}$	average error in $H_{12}^{\rm PS}$, bar
ERR	average error in x_1
ERRH	maximal error in $H_{12}^{\rm PS}$, bar
ERR	maximal error in x_1
f	fugacity, bar
' H	Henry constant har
H_{12}^{PS}	pseudo Henry constant of solute 1 in solvent 2, eq 6, bar
М	molar mass, kg mol $^{-1}$
m_{12}	gas-liquid solubility coefficient of solute 1 in
N	number of error-contributing variables
n	number of moles or number of carbon atoms
nT	total number of moles
D D	prossure har MPa kPa
D	pressure, bar, wir a, ki a
	standard pressure, 1 han
L Ds	standard pressure, 1 bar
Dntn	Bounting composition
D	roynung correction
	gas constant, 0.514 5 mor - K -
nn T	
1 7	temperature, K
	bolling point, K
I _c	critical temperature, K
T_0	standard experimental temperature, 293 K
V V	volume, m ³
$V_{\rm sys}(T_0)$	system volume at $T_0 = 293$ K, m ³
U 	molar volume, m ³ mol ⁻¹
ŪL.	partial molar liquid volume, m ³ mol ⁻¹
U_k	error-contributing variable

$v^{\circ L}$	molar	pure	liquid	volume.	m ³	mol ⁻²
v	moran	purc	IIquiu	vorume,	***	11101

- W mass of fed component, kg
- ΔW_{supply} differential mass of supply cylinder, kg
- x mole fraction in the liquid phase
- y mole fraction in the gas phase
- Z compressibility factor

 $Z_{\rm c}$ critical compressibility factor

Mathematical Notation

|x| absolute value of x

$x _{\rm PR}$	x as calculated with the Peng–Robinson equa-
	tion of state increment of x or absolute error
	$\operatorname{in} x$

Greek Letters

α_{ss}	cubic thermal expansion coefficient of stainless
	steel, $5.2 \times 10^{-5} \text{ K}^{-1}$
β	relaxation factor, eq 23
γ, γ^*	activity coefficient
Q	density, kg m ⁻³
φ	fugacity coefficient
ω	acentric factor
Subscr	ipts
i	component i
k	control variable
N_2	nitrogen

PR calculated with the Peng-Robinson equation of state

1 component 1, solute

2 component 2, solvent

Superscripts

\mathbf{E}	excess
L	liquid phase
LIT	literature value
lof	by lack of fit
\mathbf{PS}	pseudovalue
sys,rp	by systematic and reproducibility effects
V	gas or vapor phase
٥	pure component

Appendix: Experimental Data

The primary experimental measurements were P, T, the system volume at T = 293 K, and the amount of solute and solvent (here expressed in moles). The system volume at T = 293 K was always 974×10^{-6} m³. x_1 , y_1 , H_{12}^{PS} were calculated from these primary data as described above. Pntr, the Poynting factor, is defined by

$$Pntr = \exp(\int_{P^{\circ}}^{P} \overline{v}_{1}^{L} (RT)^{-1} dP)$$

The values of these parameters for 60 binaries are given in Tables A1-A60.

Table A1						Table	a A2.							Table A3						Table	: N 5.					
solute;	C02:		0.550 ((low		solut	te:	ë		0.189	(mol)			solute;	H2:		0.362 (1	10)		solu	i i i	SHSOH:	o.	646 (mol	_	
solvent;	CeH18O	3:	3.738 ((lom)		solv	ent;	CeH18O5		4.011	(mol)			solvent;	CeH1eO		3.918 (1	mol)		solv	nt: T	aH18O5:	2	579 (mol	_	
- United States of the second	4	×	, v	H ^{PS} 12	Pntr	15	_ a.	+	×	×	Ŧ	PS Pn	<u>5</u>		+ :	×"	y,	H ^{PS} 12	Pntr	un 1	۵.	H	×	×	H ^{PS} 12	Pntr
nr. bar	×	1	1	bar	1	nr.	bar	×	1	1	^	ar -	1	par	×	'	-	bar	,		bar	×	1	1	bar	,
						.								1 45.7	2 401.4	0.0058	1.0000	7527.7	1.052	1	1.35 4	125.0 0	0,1960 (. 9994	6.8 1	. 001
2 11.42	308.3	060.0 E	6 1.0000	108.8	1 015	- ~	16.58	313.3	00 00 00	1.00	00 467	0.1 7.0 8.4 1.0	22	3 47.1	9 411.3	0.0071	1.0000	6355.8	1.055	~ ~	1.20	129.7 0). 1956 (0. 9993 0. 0001	1	100
3 12.2	313.6	6 0.095	9 1.0000	119.0	1.016		16.92	318.2	0.003	1.00 1.00	00 461	1.7 1.0	នេ	4 47.9	1 416.3	0.0078	1.0000	5887.8	1.056	1 4	1.88	0 2.004	1945 (0. 9989	- -	002
4 13.1	2 318.7	7 0.094	3 1.0000	0 128.8	1.018	4	17.27	323.1	0.00	1.00	00 456	4.3 1.0	23	5 48.7	1 421.0	0.0085	1.0000	5516.4 5177 8	1.058	ŝ	2.09	444.5 0	. 1939 (0. 9987	10.5 1	. 002
5 13.9	323.7	7 0.092	8 1.0000	139.0	1.019	in v	17.62	328.3	0.00	1.00 1.00	00 442	3.1 1.0	24	7 50.1	16 430.4	0.0099	1.0000	4867.1	1.061	9	2.32	449.4 0	0.1934 (0.9984	11.7 1	. 003
7 15 41	3.05.	4 0.091 7 0.090	0000 F	157 1	1.020	0 6	11.98	333.3	0.00	00 1.00		9.8 1.0	47 47	8 50.8	33 435.5	0.0109	0. 9999	4462.2	1.062		2.55	454.3 0	0.1928 (0.9980	12.8	003
8 16.25	337.8	3 0.089	1 1.0000	1.101	1.022	~ ~ ~	18.68	343.1	000	4 1.00	00 416	3.3	55	9 51.3	36 440.6	0.0122	0. 9999	4022.0	1.063	00 C	2.83	1159.4 0 1163 0 0	0.1920 (0.9976		100
9 17.06	342.1	1 0.087	9 1.0000	178.4	1.023		19.05	348.2	0.004	6 1.00	00 407	5.2 1.0	22	10 51.8	22 445.0	0.0134	0.9999	1.683.1	1.065	ν <u>τ</u>	5.0.0	160.7 U	1001	0.9965	1 0 21	500
10 17.9	347.6	6 0.086	6 1.0000	190.7	1.024	10	19.38	352.6	0.004	7 1.00	00 401	9.1 1.0	26	12 53.2	8 454.9	0.0152	0. 9998	3325.0	1.068	21	3.65	173.7 0	0.1901	0. 9959	18.5 1	. 006
11 18.8	5 352.7	7 0.085	5 1.0000	202.5	1.025	Π	19.75	357.7	0.004	9 1.00	062 00	3.1 1.0	26	13 54.0	5 459.9	0.0163	0. 9998	3153.2	1.070	12	3.97	479.0 0	0.1894 (0. 9950	20.1 1	. 006
12 19.6		3 0,084	6 1.0000	212.7	1.026	12	20.12	362.9	0.00	1.00	00 379	4.4 1.0	27	14 54.7	76 464.	0.0173	0. 9997	2998.5	1.072	13	4.27	483.5 0	0.1887 (0.9942	21.6 1	. 007
10 20.4	369.0		9 1.000C	223.8	1.028		20.50	368.0	0.00	4 1.00	00 3/0	1.1	12	15 55.4	15 469.5	0.0184	0.9997	2849.5	1 0/4	14	4.63	188.8 0	0.1879 (0.9931	23.5	. 008
15 22.09	3.995.0	2 0.003	1 1.0000	2.45.5	1 030	a f	20.83	3 775		2 - 2 - 2 -		0 - I - O	87 00	17 26.1	14 4/4.4	0.0208	0. 9995	2575.0	1.078	15	4.95	493.4 0	0.1872 (0. 9919 2 2005	1.12 1.12	808
16 22.8	3 378.6	5 0.081	9 1.0000	255.3	1.031	16	21.59	382.5	0.006	1.00	00 342	5.7 1.0	29	18 57.5	54 483.9	0.0220	0.9993	2462.5	1.080	9 1	25.0	198.3 0 503 A 0	0.1865	CU66.0	1 0 62	600
17 23.62	383.6	5 0.081	3 1.0000	265.9	1. 032	11	21.98	387.4	0.006	4 1.00	335	0.8 1.0	58	19 58.2	25 489.0	0.0233	0. 9992	2341.4	1.083	18	- 10 9 9	507.8 0	1821 (0.9871	30.7	110.1
18 24.3	3 388.4	4 0.080	8 1.0000	1 276.0	1.033	18	22.36	392.6	0.006	7 1.00	00 324	4.5 1.0	90	20 58.9	90 493.9	0.0248	0666 .0	2225.7	1.085	19	6.42	512.5 0	0.1844 (0.9851	32.6	1.012
19 25.2	2 393.7	7 0.080	3 1.0000	287.2	1.035	16	22.74	397.6	0.00	0 1.00	00 315	7.9 1.0	31	21 59.5	28 498.2 28 503 2	2070.0 5	0.9985	2027.3	1.090	20	6.87	517.8 0	0, 1837 (). 9826	34.8 1	1.013
20 25.9	398.4	4 0.080	0 1.0000	297.0	1.036	8	23.10	402.0	0.00	3 1.00	00 308	7.2 1.0	22	23 61.0	04 508.9	0.0292	0.9982	1940.5	1.093	21	7.26	522.4 0	0.1830 (0. 9801	36.8	014
20 27 45			0000 I 4	307.0	1.03/	2 8	23.48	407.1	00.00	00-1-00 0-1-00	667 00	2.8 1.0	25	24 61.6	59 513.6	5 0.0307	0.9978	1857.5	1.096	22	7.69	527.2 0	0.1823 (0. 9772	38.9	015
23 28.15	413.2	2 0.079	4 1.0000	324.6	1.039	3 2	96 14	412.3	0000	4 1.00	282 00	9.6 1.0 4.6 1.0	2.45	25 62.4	14 518.	7 0.0324	0.9973	1778.2	1.099	53	8. I 8. 1	532.0 0	0, 1817	0702	41.01	018
24 28.8	1 418.3	3 0.079	4 1.0000	331.9	1.040	57	24.65	422.0	0.008	1.00	00 274	6.3 1.0	38	26 63.2	21 523.0	0.0340	0.9968	1/10.4	1 106		0. 0	0.000	1101 .	7.7.05	2	
25 29.4	422.9	9 0.079	6 0.9999	338.2	1.041	25	25.03	426.8	0.005	1 0.99	99 267	1.1 1.0	36	28 65.0	04 533.0	5 0.0372	0.9955	1594.3	1.111	I A CL	YV -					
26 30.0	3 427.5	5 0.079	7 0.9999	344.5	1.042	56	25.41	431.7	0.00	5 0.99	99 259	0.1 1.0	8													
2/ JU. 6 28 31.30	432.6	0.080.0	99999 U 99999 3 D 99999	350.8	1.044	12	25.83 26.21	436.8	0.010	00 0,99	99 251 99 244	6.0 1.0 2 3 1 0		Table A	÷.					solu	te;	C3H7OH:	•	.572 (mo)	-	
29 31.8;	442.6	5 0.080	7 0.9998	360.7	1.046	53	26.60	446.6	0.010	66 0 6	98 237	0.3 1.0	36	solute;	CHOOH		0.695 (m ol)		solv	ent; C	38H18O5:	~	.446 (mo1	-	
9 8 8 9 8 9 8	447	0.081	2 0.9998	365.0	1.047	88	26.99 25.99	451.4	0.01	66 0 60 0 0 0	98 230	6.3 1.0	40	solvent	: CaHtaC	:5	2.590 (1)								
32 33 41	5.75 1	9 0.081. 5 0 082	3 0 9996	308.4	1.050	38	08 17	456.2	0.012	86.0 P	96 217	4.0 	19								٩	F	,	>	rPS H	Phtr
33 33.91	462.6	0.0830	0 0.9995	373.7	1.051	38	28.21	466.3	0.012	66 0 6	95 210	9.4 1.0	100							n	-	•	- -		.12	
34 34.3	467.4	1 0.083	2 0. 9993	375.8	1.052	34	28.56	470.6	0.013	M 0.99	94 205	4.2 1.0	44	run P	T	×	۲ <mark>،</mark>	H ^{PS}	Pntr	лг.	bar	X	I	I	bar	ı
35 34.8	472.2	2 0.084	4 0.9992	377.2	1.053	83	28.95	475.3	0.014	66 °0 01	92 199	8.8 1.0	4 5	nr.				1.4		.						
2 2 2 2 2 2 2	1 100 1	0 0.085	2 0.9990	378.6	1.055	85	29. 38 20. 70	480.4	0.014	10 0.99 3 0.99	90 193 92 193	7.6 1.0	47				1				0.80	433.3 (0.1866	0.9984 0.9980	4 4	1.000
38 36.05	1 487 0	00000	0.9984	5.675 5.975	1 057	5 8	67.63 66.06	490.5	0.015		85 187		¢ ;	1 1.3	80 430.	7 0.2060	0.9994	8.6	1.001	v (*	1.04	443.1 (0 1859	0.9976	i un	1.000
39 36.44	491.9	9 0.087	9 0.9980	378.6	1.059	6	30.61	495.4	0.016	6 0 9	81 176	5.8 1.0	51	2 C	00 435.1	8 0.2054	0.9992	9.6	1.002	4	1.19	448.4	0.1854	0.9971	6.9	1.000
40 36.75	497.0	0.089	0 0.9976	376.9	1.060	40	31.03	500.3	0.017	.3 0°.99	77 171	4.9 1.0	53	. 4	47 445	5 0.2042	0.999U	11 8	700	ŝ	1.33	452.3 (0.1850	0. 9968	7.0	1.001
41 37.01	3 501.4	0.090	0 0.9972	376.2	1.061	4	31.45	505.0	0.015	0.99	72 166	8.0 1.0	54	5.2.	73 450.0	3 0.2035	0.9986	13.1	1.003	9	1.47	457.9 (0.1846	0. 9960	7.8	1.001
2.15 24	5 FOC 2	060.0	4 U.9969	375.5	1.062	35	18.16	510.0	0.015	80°0 90°0 90°0	56 161 57 157	6.1 1.0 1.0	9, 0	0 10 10	98 454.8	8 0.2029	0.9983	14.3	1.003	~ 0	1.02	462.1	0.1841	U. 9955 D. 9945	o v n o	1.002
10.10 04		0.076	1 v. 7747	3/4.1	1.000	44	32.26	519.6	020 0	66 0 1	2 C 2 C 2	- - - - -	89	- a	27 459.	0.2022	0.9979	5.7	1.004	• •	1.97	471.9 (0. 1832	0.9935	10.4	1.002
						45	33.11	523.7	0.021	1 0.99	44 148	7.6 1.0	61	, 	88 469.4	1 0.2008	0.9970	11	1.005	10	2.15	476.4 (0. 1827	0.9924	11.4	1.003
						46	33.54	528.3	0.021	9 0.99	34 144	7.4 1.0	64	10 4.	19 474.3	0.2001	0.9964	20.2	1.006	11	2.38	481.6 (0.1821	0. 9911	12.6	1.003
						47	33.60	528.8	0.022	0 0.99	33 144	4.6 1.0	64	11 4.5	55 479.0	3 0.1993	0.9956	22.0	1.006	12	2.60	486.6 (0. 1815	0. 9895	13.7	1.004
														21 2 7 7 7	55 483.3	9 0.1986	0.9949	23.6	1.007	: : :	2.83	491.5 (0.1810	0.9878	14.9	1.005
														14 5.6	55 493.9	0.1970	0. 9928	27.4	1.008	4	36	196.4	0.1804	0.9858	0	
														15 6.0	02 498.0	3 0.1963	0.9917	29.2	1.009	c1 91	5. 19 19	505.9	0. 1793 0 1793	0.98.30 0.9812	18.7	001. 1.00
														16 6.4	10 502.9	0.1956	0. 9903	31.0	1.010	17	3.81	510.5	0.1787	0. 9785	20.0	1.007
														11 0.2	58 508. 32 513.(0.1947	0. 9868	3.5	1.011	18	4.10	515.5 (0.1781	0.9753	21.5	1.008
														19 7.8	30 517.9	0.1931	0.9847	37.9	1.013	19 20	4.40 1 58	520.5	0.1775	0.9716 ^ 0490	23.0	1.009
														20 8.2	27 522.5	0.1923	0.9825	40.1	1.014	21	5.01	530.1	0.1764	0.9634	26.0	1.011
														22 9.3	14 261.1 33 532.6	0.1907	0. 9768	46.4	c10.1	22	5.34	535.0 (0.1758	0.9584	27.6	1.012
														23 9.8	38 537.0	0.1899	0.9737	47.9	1.018	23	5.66	539.2 (0.1753	0. 9539	29.2	1.012
														24 12.6	57 557.2	0.1861	0.9571	60.9	1.026	24	6.03	544.4 (0.1747	0.9476	6.0°	1.014

Table A7.						Table	. A 9.						Table	M1.					Ta	ble A13					
solute:	C4H9O	H: C).585 (mol	-		solut	e; H	:02	J).615 (mc	(1,		solute	ë			0.2	23 mol	50	lute;	CH3OH		0.289 (1	01)	
solvent;	CeH18O5		2.425 (mol	-		solve	int; C	aH1805:	^{(N}	2.291 (mc	(10		solven	t; C10	H14:		3.8	99 mol	so	lvent;	C10H14		3.843 (n	ol)	
run P nr. bar	H X	×")	, r	H ^{PS} 12 har	Pntr	n. Tu	P bar	+ ×	×"	y, -	H ^{PS} 12 bar	Pntr -				v	Da H ^P	s Phti		п. bar	н м	×"	r <mark>,</mark> -	H ^{PS} 12 bar	Pntr
	{	,	-	IPO	,								- 3	94 440	0	75 0 00	.000		 .	2.80	425.9	0.0641	0. 9981	42.3	1.003
1 1.15	5 453.8	0.1904	0.9960	5.91	000	- 2	1.41 1.54	449.9	0.2061 0.2056	0. 9975 0. 9971	6.8 7.4	1.000	23.	10 460	0.0	81 0.95	89 2772	6 1.03	2 6	2.98	430.6	0.0638	0.9978	45.2 AB A	1.004
3 1.46	463.2	0. 1895	0. 9945	7.4 1	100	~~ •	1.73	458.3	0.2050	0.9966	8.3	1.001	4 23.	40 465 63 469	0.0	182 0.99 184 0.99	87 2761 85 2714	.1 1.03	~ ~ ~	3.38	440.4	0.0632	0.9970	51.7	1.004
4 1.60 5 1.79	3 468.4 1 477 8	0.1891 0.1886	0.9935 0.9935	8.3 1	(. 002	a 10	2.12	403.4 468.4 (0. 2038	0. 9952 0. 9952	9.2 10.3	1.001	5 23.	93 474	90.0	86 0.99	83 2693	9 1.03	5 Y	3.60	445.4	0.0629	0.9966 0.9961	55.3 58.6	1.005
6 1.95	477.2	0. 1882	0.9913	9.9	. 003	y t	2.37	473.5	0.2030	0.9943	11.4	1.001	0 24. 7 24.	43 483	00.0	88 0.99 89 0.99	80 2654 77 2642	1 1.039	• •	4.01	455.1	0.0623	0.9955	61.9	1.005
7 2.16 8 2.37	5 482.6 1 487 5	0.1876 0.1871	0.9897 0.9881	11.0	. 003	~ 00	2.82 2.82	483.4 (0.2023	0.9922	12.5	1.002 1.002	8 24.	73 489	.3 0.00	92 0.99	73 2607	1 1.041	@ 0	4.24	460. 1 464 6	0.0620	0.9948	65.8 69 1	1.006
9 2.56	491.8	0.1867	0.9864	13.0	. 005	6;	3.13	488.2	0.2007	0.9911	15.2	1.002	9 24. 10 25.	97 494 26 498	0.0	1941 0.99 1966 0.99	69 2569 65 2547	9 1.042	2	4.68	469.6	0.0614	0.9933	73.1	1.007
10 2.8.	3 497.3	0.1860	0.9840 0.9816	14.3 1	005	2 =	J. 45	493.3	0.1989	0. 9879	16. / 18. 4	1.003	11 25.	53 503	.8 0.00	66.0 86	60 2511	1 1.040	==	4.91	474.4	0.0611	0.9924	76.7 80.6	1.007 1.008
12 3.34	1 506.9	0.1848	0.9791	16.8 1	. 007	12	4.08	503.0	0.1980	0.9862	19.9	1.004	12 25. 13 26.	/8 508 05 513	. 5 0.01 . 6 0.01	00 0.99 03 0.99	55 2475 48 2431	2 1.044	15	5.37	484.2	0.0606	0.9904	84.5	1.008
13 3.58 14 3.88	8 511.0	0.1843	0.9733	18.0 1 19.5 1	008	14	4.86	513.0 (0.1970 0.1960	0.9820	23.8	1.005	14 26.	31 518	0 0.01	05 0.99	42 2410	2 1.046	14	5.61 5.83	489.2	0.0603	0.9891	88.5 92.0	1.008 1.009
15 4.16	520.6	0.1830	0.9699	20.9 1	600 .	15	5.28	517.9	0.1949	0.9797	25.9	1.005	15 26. 16 26.	58 523 87 528	0.01	07 0.99 10 0.99	35 2370. 77 2342	0 1.047	16	60.9	498.8	0.0598	0.9864	96.4	1.009
16 4.55 17 4.98	525.8	0.1822 0.1813	0.9657 0.9612	24.7	011	17	6.28 6.28	528.1 (0.1936 0.1924	0.9740	4.87 90.9	1.006	17 27.	16 533.	0 0.01	12 0.99	18 2310	8 1.049	18	6.34	503.7 508.4	0.0596	0.9848 0.9832	100.5 104.3	1.010 1.010
18 5.36	535.9	0.1805	0.9566	26.6	.013	18 19	6.80 7.36	532.9	0.1911 0.1898	0. 9709 0. 9674	33.5 36.4	1.007 1.008	19 21	150 14	8 0.01	15 0.99	08 2276.	5 1.050	-1	6.83	513.4	0.0591	0.9813	112 8	1.011
																			212	7.34	523.2	0.0587	0.9771	116.8	1.012
Table A8.						Table	5 A10.						Table /	12.					22	7.63	528.3 533.2	0.0585	0.9746 0.9720	121.6 125.4	1.013 1.013
solute:	CsH11	OH: I	0.445 (mol	0		solut	e:	CO2:	-	D.450 (m	(lc		solute;	H2:		0. 397	(10) (10)		24	8.16	538.3	0.0581	0.9692	129.9	1.014
solvent;	CeH1 805		2.368 (mol	2		solve	int;	C10H14:		3.922 (m	01)		solvent	Ciol	h4:	3.860	(loul)		Ta	ble A14					
				ž			<u>م</u>	L L	×	>	54H	Pntr		T	×	Y	* ±	Putr	50	lute;	C2H5OH		0.337 (#	ol)	
run P	н	×「	y, 	H ¹²	Pntr	nur.	bar	×	- 1	7 1	bar	.		¥	- 	-	pa	'	so	lvent;	C10H14		3.843 (∎	01)	
bar	×			bar		-	1 38	9.99.9	0.0491	0. 9999	455.4	1.036	1 33.	39 405	.6 0.01	66 0.99	99 1943	2 1.04	 _	•	⊢	,	>	нРS	Putr
1 0.8	0 453.1 3 458.2	0.1550 0.1550	0.9943 0.9924	5.1 5.0	0. 999 0. 999	• ~ ~	5.22	407.4	0.0487	0.9998	475.8	1.038	2 33.	88 410 34 415	.7 0.01	67 0.99 69 0.99	99 1956 99 1961	5 1.044	25	. <u>}</u>	• •	-	<u>,</u>	12	
30.0	1 463.0	0.1550	0. 9903	5.1	0. 999	ייי קריי	29. 31 26. 31	412.0	0.0482	0. 9997	501.4	1.039	4 34.	82 421	0.010.01	71 0.99	98 1970	9 1.045		Dar	4		ŧ		
4 0.9	0 467.9 2 472.5	0.1547 0.1544	0. 9886 0. 9871	5.7 6.4	1.000	in u	26.76	422.1	0.0481	0.9997 0.9996	511.1	1.040	5.35. 35.35	27 426 51 428	.0 .7 .0	73 0.99 74 0.99	98 1970 98 1970	3 1.046		2.31	427.1	0.0761	0.9976	29.4	1.003
9 1.0 9	9 475.0	0.1542	0.9862	9 9 9	1.000	2	27.82	432.1	0.0478	0, 9995	534.9	1.042	7 36.	14 436	.4 0.01	79 0.99	97 1947	4 1.048	. e	2.63	435.9	0.0756	0.9969	33.6	1.003
8 1.4	1 487.1	0.1532	0. 9804	0 00 0 00	1.001	00 ON	28. 33 28. 78	437.2 441.9	0.0477 0.0478	0. 9994 0. 9993	545.9 554.1	1.043	8 9 9 7 8 9	61 441 06 446	.4 0.01	83 0.99	96 1950.	3 1.050	4 0	2.82 2.99	440.9 445.7	0.0753	0.9965	36.2 38.3	1.00 4 1.00 4
9 1.5 10 1.6	5 492.2 9 496.3	0.1528 0.1524	0.9747	9.6 10.5	1. 002 1. 002	9	29.28 10.75	446.8	0.0477	0.9992	564.8 573.7	1.045	10 37. 11 37.	48 451 94 456	.2 0.01 10 0 10	85 0.99 88 0.99	95 1947. 94 1940	0 1.051	9 1	3.17	450.7	0.0748	0.9953	40.8 42.5	1.005
11 1.8	6 501.3	0.1520	0.9711	11.5 12 6	1.003	12	30.23	456.5	0.0477	0.9988	582.8	1.047	12 38.	37 461	10.0	66 0 06	93 1938	4 1.05	- 00	9.58 	460.4	0.0742	0.9939	46.2	1.005
13 2.2	5 510.9	0. 1509	0.9635	13.8	1.004	11	30.72 31.22	461.5 466.6	0.0477 0.0478	0.9986	592.0 600.7	1.049	14 39.	81 460 25 471	0.01	95 0.99	92 1928 90 1922	9 1.055	6 01	3. 77 4. 01	464.7 469.9	0.0740	0. 9932 0. 9923	48.7 51.9	1.006 1.006
14 2.4 15 2.6	4 515.1 5 519.9	0.1504 0.1499	0.9597 0.9548	14.9 16.2	1.005 1.005	15	31.64	470.8	0.0478	0.9982	608.4 616.7	1.050	15 39. 16 40.	67 475 09 480	0 0 0 L	99 0.99 01 0.99	89 1909. 87 1902	6 1.056 1 1.057	11	4.22	474.7	0.0734	0.9913	54.7	1.007
16 2.9	2 524.7	0.1492	0.9499	17.7	1.006	11	32.65	481.1	0.0480	0. 9976	625.0	1.052	17 40.	51 485	.5 0.02	05 0.99	85 1888	9 1.058	13	4.68	484.0	0.0728	0.9892	6.09	1.008
17 3.2 18 3.5	6 534.7 8 534.7	0.1484 0.1476	0.9391	21.5	1.009	8 6	33, 13 13, 59	486.2 490.9	0.0481 0.0483	0. 9972 0. 9968	632.5 639.2	1.053	18 40. 19 41.	95 490 39 495	. 4 0.02 . 4 0.02	07 0.99 11 0.99	83 1882 80 1868	8 1.060 5 1.061	14	4.89	494.3	0.0726	0.9879 0.9864	63.7 67.6	1.008 1.009
						28	34.02	495.4	0.0484	0.9964	645.3	1.055	20 41.	80 500	0 0.02	14 0.99	77 1857	4 1.062	19	5.41	499.1	0.0721	0.9848	70.6	1.009
						5 2	34.51 34.95	500.5 505.4	0. 0486 0. 0488	0.9959	651.9 656.7	1.056	21 42. 22 42.	62 510 65 510	0.02	21 0.99	70 1824.	1 1.065 6 1.065	17	5.67 5.93	504.1 509.0	0.0718 0.0716	0.9831	74.1	1.010 1.011
						52 7	35.47 35.91	510.5	0.0489 0.0492	0.9948 0.9942	664.2 668.3	1.059	23 43. 24 43.	07 514 49 519	.7 0.02	25 0.99 28 0.99	67 1813. 62 1798.	0 1.066 3 1.067	202	6.18 6.44	513.8	0.0713	0.9794 0.9772	80.8 84.2	1.011
						52	36. 33	520.0	0.0494	0.9935	672.6	1.062	25 43.	89 524	2 0.02	32 0.99	58 1781	6 1.065	121	6.69	523.3	0.0709	0.9750	87.4	1.012
						26	36.83	525.0 530.2	0.0496 0.0499	0.9927 0.9918	678.1 682.4	1.063	20 44. 27 44.	75 534	3 0.02	41 0.99	52 1/65 46 1745	0 I.U// 3 1.072	22	6.96 7.22	528.0 532.9	0.0707	0.9726	90.9 94.3	1.013
						58	37.76	534.8	0.0501	0.9909	686.1	1.066	28 45.	15 539	1 0.02	45 0.99	40 1725	1 1.073	12	7.49	537.9	0.0703	0.9670	97.8	1.014

Table A15.					Tab	le A17.						Tabl	e 119.						Table	A20.					
solute;	C3H70H:	0.389	(m ol)		sol	ute;	CsH	HOIL	0.382 (1	(lo		solu	ite;	ë	0	.554 (mo	1)		solut	e; H	ŝ	0.60	5 (mol)		
solvent;	CioH14:	3.832	(mol)		so1	vent;	CioHi	÷	3.389 (⊪	(lo		solv	ent;	C16H34		om) E00.	(1		solve	nt;	C16H34:	2.10	5 (mol)		
run nr. bar	× י	ין א <mark>ז</mark>	H ^{PS} 12		n .	<u>ا</u> م	н 1	×"	×.	H ^{PS}	Pntr			⊢	×"	×,	H ^{PS} 12	Pntr	n i	<u>م</u>	F	×"	"H	5 2 5	뉟
	4		nai			Dar	-	1	I I	bar	•		bar	К	1	I	bar	ı	L	bar	K	-	pa	-	
1 1.23 2 1.36	426.6 0.0 431.4 0.0	900 0.996(397 0.9955	0 13.4 5 14.8	1.001 1.001	5 -	1.03 1.12	463.9 468.9	0660.0	0.9771	10.0 10.8	1.000	7 7	31.37 31.76	301.0	0.0466 0.0466	1.0000	623.0 615.1	1.066	1 3	7.99 3 7.42 3	01.0 0.1	0337 1.00	000 1068	8.4 1.0 5.1 7.0	890
3 1.48 4 1.60	441.4 0.00	896 0.9948 394 0.9941	3 16.0 17.3	1.001	↔ 4	1.24	473.8	0.0986	0.9753	11.9	1.001	. n .	32.38	310.6	0.0490	1.0000	611.7	1.068	າຕ 1 ຕ	16: 16: 16:	09.2 0.0	0364 1.00	000 1000	.4 1.0	220
5 1.73	446.2 0.01	392 0.993	1 18.8	1.002	ימי	1.44	483.3	0.0983	0.9706	13.8	1.001	4 V	33.41	315.4 0 319.7 0	0.0501	0000	608.8 607 9	1.069	ო ი ო ს	9.42 3 9.96 3	13.1 0.1 17.3 0.1	0373 1.00 0383 1.00	000 987 000 983	8 1.0	120
6 1.89 7 2.02	456.1 0.05	590 0.9925 388 0.9916	20.4	1.002	9 6	1.56	488.3	0.0981	0.9679	14.9	1.002	9	33.97	324.5 0	0.0519	1.0000	606.2	1.072	6	0.55 3	21.7 0.0	0392 1.00	62.6 000	9.8 1.0	174
8 2.17	460.5 0.00	386 0. 9907	23.5	1.003	- 00	1.81	497.9	0.0976	0.9624	17.2	1.003	~ 8	34.68 35.23	330.7 C	0.0532	1.0000	603.6 601.5	1.074	- 8 4 4	1.18 3 1.77 3	26.4 0.1	0402 1.00	000 954 000	8.8 1.6 1.0)76 777
10 2.50	465.5 0.05	384 0.9895 382 0.9883	25.3	1.003	6 Q	1.94 2.08	502.9	0.0974	0.9591	18.4	1.003	6	35.76	340.2 0	0.0552	. 0000	599.0	1.077	6	2.37 3	35.2 0.6	0422 1.00	000 942	.4 1.0	620
11 2.67	475.3 0.06	380 0.9870	29.0	1.004	2 =	2.24	512.7	0.0970	0.9524	21.1	1.004	2 2	36.38 36.38	345.6 0 350 0 0	0.0564	0000	596.3 502.0	1.079	10 4	3.12	40.7 0.0	0433 1.00	000 932 000 932	1.1	181 Pe 1
12 2.86 13 3.02	480.3 U.U. 484.7 0.06	377 0.9856 176 0.9841	31.0	1.005	12	2.38	517.5	0.0968	0.9487	22.4	1.005	12	37.48	355.2 0	0.0586	. 0000	590.7	1.083	12 4	1.56	51.4 0.0	0459 1.00	906 000	.8 1.0	85
14 3.23	490.0 0.05	373 0.9823	35.0	1.006	1	2.72	527.3	0.0963	0.9408	25.4	1.000	<u> </u>	38.07 38.64	360.4 0 365.4 0	0.0597	0000	587.7 584 2	1.085 1.087	13 4 4 4 4	6.03 6.83 6.83	55.3 0.0 50.8 0.0	0468 1.00 0482 1.00	000 898 000 884	0.1.0 1.0	087 089
15 J.42 16 J.64	500.2 0.05	5/1 U.9805	39.0	1.006	51	2.88 70	532.1	0.0961	0.9364	26.8	1.006	15	39.20	370.4 0	0.0621	. 0000	580.5	1.089	15 4	6.43 3	55.3 0.0	1.00	000 874	1.5 1.0	160
17 3.86	505.0 0.06	367 0.9763	41.6	1.007	17	3.28	542.0	0.0956	0.9275	30.2 30.2	1. 007	16	39.72	375.0 0	0633	. 0000	576.8	1.091	16 4	7.08 3	70.2 0.0	0507 1.00	000 861		94
18 4.06 19 4.28	509.9 0.06	365 0.9739 163 0.9736	43.8	1.008								81		385.3 0	0000	0000	568.1	1.095 1.095	18	. SS	31.2 0.0	1.00 1.00	000 834	0.1 0.1	66
20 4.51	519.7 0.05	161 0.9687	48.4	1.000								19	11.32	389.3 0	. 0671	. 0000	564.6	1.097	19 4	0.14 3	35.6 0.0	549 1.00	00 824	9 1.1	10
21 4.72	524.4 0.05	159 0.9659	50.6	1.009								212	12.53	94.8 0 100.2 0	2890 . 0201	0000	559.7	1.100	22 23	56. 192 192	91.6 0.0 96.0 0.0	579 1.00	000 811	0.1.1	04
22 4.96 23 5.19	533.9 0.05	357 0.9630 355 0 9599	53.1	1.010	Tab	A18						5	13.10	105.4 0	.0716	6666 '	549.0	1.105	22 5	1.32	01.9 0.0	1.00	00 786	.3 1.1	3 2
24 5.44	539.0 0.08	153 0.9563	28.0	1.011			, troo		-, 000 0	-		53	13.54	109.4 0	0728	. 9999	544.9	1.107	33	0.02	0.7.3 0.0	0613 0.99 2025 0.99	ETT 990	1.6	£13
									L 205.0	(10		55	14.74	0 0.61	0160	6666	533.7	1.110	6 in 52 7	9.11 9.11	1.2 0.0	641 0.99	CO 1 661 661 661 661 661 661 661 661 661		<u>e</u> 2
					105	/ent;	C10H14	<u></u>	3.394 (m	01)		26	15.08	24.8 0	0780	6666 .	523.4	1.116	52 58	9. 77	20.6 0.0	656 0.99	141 66	.7 1.1	22
										2		27 28	15.61 4 16.20 4	29.7 0	.0795 (99998	518.2	1.119	5 2 5 2 7 2	1.52	26.3 0.0	675 0.99	99 728	.5 1.1	52
Table A16.					run	~	т	×	۲ ₁	H ¹²	Pntr	3 62	16.72 4	40.0	.0828 0	8666 .	507.2	1. 125 1. 125	5 75 5 8	- 14 - 18 - 14	36.5 0.0	710 0.95	111 66 98 705	4 1.1	ខ្ល
solute;	C4H9OH:	0.465 (mol)		пг.	bar	¥	1	1	bar	1	85	7 20 4	45.2 0	.0845 0	79997	501.5	1.129	15 14 16 75	51 4	11.4 0.0	7127 0.99	98 694 00 505	8 1.1	36
solvent;	CioHi4:	3.389 (mol)		-	3.61	419 g	0 0727	0000	V OV	000	58	8.33	55.0 0	0878 0	9666 ·	490.7	1.132 1.136	2: n 35 n	9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	51.2 0.0	762 0.99	cao 86	- 1- 1 - 1- 1 - 1- 1	4 4
					• 0	4.00	424.8	0.0717	0. 9987	54.3 54.3	1.003	8.5	8.78 4	59.2 0	0 6680.	9666 .	486.0	1.139	83	3. 47 45	56.3 0.0	780 0.99	94 663	.2 1.1	48
run P	T ×	۲,	H ⁷⁵	Pntr	ლ -	4.32	430.0	0.0709	0.9985	59.1	1.004	4 K	4 06.6	64.8 69.9 0	0 1260.00	. 999 4	473.5	1.144 148	5 6 5 6	0.78 9.78	5.3 0.0	1798 0.99 1818 0.99	97 653 96 641	. 4 1.1 . 8 1.1	22 22
nr. bar	' ×	I	bar	1	ιΩ	4.87	439.6	0.0697	0. 9979	67.6	1.004	36.5	0.42 4	74.8 0.	0949 0	1 666	467.9	1.152	88	.31 40	0.0	835 0.99	96 632	1.	19 3
					9 1	5.16	444.7	0.0690	0.9976	72.1	1.005	58	1 48 4	0 0 0 0 0 0 0 0 0	0 4960. 0 4960	5666 . 2000	463.2	1. 156	6 4 7 8	- 02 - 02		878 0.99	079 06		8 6
1 1.10 2 1.23	446.3 0.11 451.5 0.11	79 0.9892	10.1	1.000	~ 8	5.71	454.2	0. 0679	0. 9972 0. 9968	76.3 81.1	1. 005 1. 005	6.5	- 7 - 00 - 7	89.7 0.	1004 0	1666	450.9 1	1. 166 I. 166	8 8 8 8 8	50 17 17	2.3 0.0	893 0.99	94 601	. 8 . 1. 1	76
3 1.36	456.2 0.11	TT 0.9882	11.2	1.001	6 Ç	5.99	459.2	0.0673	0.9963	85.6	1.006	41 5	2.95 4	94.3 98.4 0.	0 1201 0	0666	446.0	1. 171 176	6 6 6 6	. 52 4	1.0 0.5 0.0	66 0 926	92 581 92 581	2.1.1	82
5 1.60	465.7 0.11	73 0.9856	13.0	1.002	2 Ξ	6.56	469.1	0. 0662	0.9951	95.0	1.006	42 5	3.49 5	03.6 0.	.1058 0	8866	434.9 1	1.182	42 64	. 06	9.8 0.0	953 0.99	91 573	.1 1.1	92
6 1.74	470.5 0.11	70 0.9842	14.2	1.002	12	6.83	473.7	0.0658	0.9945	99.5	1.007	6 4 4 2 4 4	0 26.F	0	1000	7866	430.0	1. 187	20 40 70 40	20 20 20 20 20 20 20 20 20 20 20 20 20 2		972 0.99	90 564 99 554	.5 1.1	8 2
7 1.88 8 2 02	475.1 0.11 479 9 0 11	68 0.9828 65 0 9811	15.3	1.003	13	7,08	478.4	0.0653	0.9938	103.7	1.007				0 0601	99866	120.3	192	é F	ň 61 -		983 0. 23	100 60	2 1 2	3
9 2.17	484.7 0.11	63 0. 9793	17.7	1.003	15	7.64	488.3	0.0644	0. 9920	113.2	1.008														
10 2.35	490.0 0.11	60 0.9772	19.1	1.004	16	7.92	493.3	0.0640	0.9909	117.8	1.008														
11 2.52	494.5 0.11 499 1 0 11	157 0.9754 55 0 9733	20.5	1.004	18	8.16 8.44	497.8 503.0	0.0636	0.9898	121.9	1.008														
13 2.85	503.7 0.11	52 0.9710	23.0	1.005	19	8.72	508.0	0.0629	0.9870	131.3	1.009														
14 3.06	508.8 0.11 512 5 0.11	49 0.9684	24.7	1.006	50	8.97 0.22	512.8	0.0626	0.9855	135.5	1.010														
15 3.48	518.6 0.11	44 0.9629	27.9	1.007	22	9.46	522.4	0.0621	0.9820	143.5	1.010														
17 3.67	523.4 0.11	41 0.9597	29.4	1.008	23	9.72	527.1	0.0618	0.9802	147.7	1.011														
18 J.71	533.2 0.11	35 0.9532	32.9	1. 009	3 8	7. 20	537.0	0. 0612	0. 9757	156.6	1.011														
20 4.35	537.9 0.11	33 0.9496	34.6	1.010	26	10.55	542.0	0.0610	0. 9732	161.2	1.012														

																			Ta	ble A24						
																			So	lute;	CsH	12:		0.379	mol	
																			so	lvent;	Ciel	H34:		2.018	mol	
Table A2	1.					Table	A22.					•	Table /	V2 3.					I		1			54.		
solute;	C02:		0.533 (mo	(10		solut	; ;	C2H6	0	614 (mol	~		solute;	3	먥	0.42(5 (mol)		n.	<u>ר</u> .	- :	ׯ	۲ <mark>1</mark>	112 1		
solvent;	C16	sH34:	2.102 (mc	(16		solve	nt;	C16H34:	1.	890 (mol	~		solven	- -	C16H34:	1.89	1 (mol)		:	bar	-	1	l I	bar	1	
																				1.12	396.3	0.1545	0. 9992	7.1	1.000	
٩.	Н	×	>	н ^{р5}	Pntr		٩.	Т	×	>	H ^{PS}	Patr	-	0	T×	Y	H	PS Pnt	tr 2	1.23	401.7	0.1543	0.9991	8. a	1.001	
un l		-	-	12		Ē	1		-	 -;	12			1		-1		1	• ◄	1.43	411 2	0.1538	0.9988		1 0002	
nr. bar	×	ł	ı	bar	ł	лг.	bar	Х	1	ſ	bar	1	ۆ 	ar ;	× ۱	1	ă	ar -	r vo	1.56	416.5	0.1536	0.9986	6.6	1.002	
																			。 	1.69	421.9	0.1533	0.9983	10.7	1.003	
1 12.4	2 305.1	7 0.1453	1.0000	78.3	1.024	-	7,02	307.6 0	. 2101 1	. 0000	31.1 1.	.016	, i 1	05 30	2.0 0.1	720 1.00	00	1.5 1.00	2 20	1.83	427.3	0.1530	0.9981	11.5	1.003	
2 12.8	309.8	8 0.1443	1.0000	81.6	1.025	~	7,41	311.7 0	. 2087 1	.0000	33.0 1.	. 017			6.1 0.1	70.1.0	000	2.4 1.00	04 8	1.96	432.1	0.1528	0.9978	12.4	1.004	
. 13. 5	6 314.6	6 0.1432	1.0000	85.4	1.026	с, •	7,85	316.2 0	. 2071 1	0000	35.2 1	.018	יי היי	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.1	/06 1.01			6 9	2.10	437.1	0.1525	0.9975	13.3	1.005	
5 1 7 S).4Iv C	0 0.1422	1.0000		1.02/			321.2 0	1 2055	0000	37.6 1.	. 020	in ru			690 1.00			2 2	2.24	441.7	0.1523	0.9972	14.2	1.005	
- 14 - C	1 323. 1	7 0 1403	1.0000	9.76	1.028	n u		0 6.025	1 1606	0000.	40.3 1	120.	i ri o o	- 10 - 10	5.1 0.1	680 1.00	00	7.1 1.00	11 20	2.35	446.8	0.1520	0.9968	12.1	1.006	
7 15.4	333 4	1991.0	1.0000	101 0	1 031		000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2005		1 4 2 4	720.	7 3.	20 33(0.1	672 1.00	11	8.3 1.00	37 12	2.53	451.8	0.1518	8 0.9964	16.0	1.006	
8 16.1	1 340 1	0 1 183	1 0000	106.3	1 012	÷α	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 9 1 PC	1 0002 1	0000		120	8 3.	45 33	5.9 0.10	663 1.00	00(9.8 1.00	38	2.2	457.1	0.1516	0.9960	1/.0	1.00/	
9 16.8	346 6	5 0 1375	1 0000	111 6	1 034	 			1 979 1	0000	1 0 03	. 026	С	71 34	1.1 0.1	654 1.00	100	1.3 1.00	2 S	2.86	462.2	0.1514	2266 0 1	18.0	1.008	
10 17.2	2 350 6	5 0.1370	1.0000	114 7	1 035	1 0	5 CC 5 CC 5 CC	151 1 0	1 2/21 -		1 0 02	020	10 3.	98 34(5.7 0.1	644 1.00	00	3.0 1.00	30	20 m c	467.0	0.1512	0666.0	19.0	1.009	
11 17.6	5 354 7	7 0.1365	1.0000	118 0	1 0.36	1 1	32.1	355 2 0	1956 1		1 0 22	020	11 4.	19 35(0.10	637 1.00	00	4.2 1.01	9] ; 10		- 2/6	0.1510	0.9944	20.2	1. 009	
12 18 2	1 960 1	1 0 1360	1 0000	122.2	1 038	1 1	2 20	0 3.000	1 0001	0000	0.02	620	12 4.	46 350	5.0 0.1	628 1.00	100	5.9 1.01	11	ต์ (ต่	477.4	0.1508	0.9939	21.3	1.010	
11 18 7		0.1357	1 0000	125.8	1 039	1	- CA 10 C	0 0.00 0 1 990	1 0501	0000	1 6.70	150.	13 4.	75 36	1.4 0.1	519 1.00	2.2	7.7 1.01	12	3.51	482.2	0.1506	0.9933	22.4	1.011	
10 19 21		1321 0 2	1 0000	129.3	1 040	2		0 0 1.000	1 0201	0000	1 0.00	760	14 4.	98 36	5.6 0.16	612 1.00	100	9.2 1.01	119	3.74	486.7	0.1505	0.9927	23.4	1.012	
15 19.7	1 176 5	7 0.1351	1.0000	133.0	1 042	: ÷		0 0 575	1 0101			100	15 5.	31 37	1.3 0.10	602 0.95	.E 660	1.2 1.01	14 20	# : 	C.244	0.1503	0.9919	24.0	1.013	
16 20.2	379.5	3 0.1349	1.0000	136.4	1.043	16	4.36	381.2 0	1901 0	66666	68.8	250	16 5.	56 37:	5.8 0.1	595 0.95	3C 66t	2.8 1.01	14 21	01.4 A	8.06	1502	0 0000	8.0	1.015	
17 20.7	3 384.4	1 0.1347	0. 9999	140.1	1.045	17 1	4.89	386.4 0	. 1892 0	6666	71.5 1.	660	17 5.	90 38	1.6 0.1:	585 0.95	Ϋ́E 66t	4.9 1.01	16 25		2005	0 1500	7989 0 0	1.80	1 016	
18 21.2	5 389.7	7 0.1346	0, 9999	143.8	1.047	18 1.	5, 39	391.5 0	.1884 0	6666 .	74.2 1.	040	18 6.	14 38	5.7 0.1	579 0.99)E 66t	6.4 1.01	16 24	4 2 4	510.8	0.1499	0 9890	4.62	1.017	
19 21.8	394.5	9 0.1346	0.9999	147.4	1.048	19 1:	5, 81	395.7 0	. 1878 0	6666 .	76.4 1.	042	19 6.	40 39	1.6 0.1:	570 0.95	108 107	8.6 1.01	81 21							1
20 22.2	7 399.6	5 0.1346	0.9999	150.5	1.050	20 1	6.26	400.2 0	. 1872 0	6666 .	78.7 1.	043	20 21 21	.75 39(6.0 0.1	564 0.9	16 41	0.3 1.0	18							
21 22.7	6 404.5	5 0.1347	0.9999	153.5	1.052	21 1.	6.74 4	405.0 0	. 1867 0	8666 .	81.2 1.	045	 	02 04 04 00	1.0 0.1	557 0.95	198 4.	2.2 1.0	22,20							
22 23.2	8 409.5	9 0.1349	0.9998	156.8	1.054	22	7.35	411.3 0	. 1861 0	8666 .	84.3 1.	047			0.2	250 U.9.		4.3 1.0	12							
	5 414.6	6 0.1352	0.9998	159.5	1.055	53 53	7, 80	415.9 0	. 1857 0	8666 .	86.6 1.	049		11 00		14.0 0.40 200 0 002	4 10 10 1	0.0 1.0 20	22							
24.2	2 419.5	0.1354	0. 9998	162.2	1.057	24	8, 22	420.2 0	. 1854 0	- 666	88.7 1	051		11 00	1.0 0.0	7.0 0 VC2	105 4	1.7 I.U.	ς Γ	ble A25						
7.1-7 7-7-7 7-7-7	2 424.6	8661.0 9	1666.0	165.1	1.059	 3 2	8,69 8,69	424.9 0	. 1851 0	. 9997	91.0 1.	052	5 9 9 0	107 22	1.0 0.1	528 0 90 5	- 15 15	7.0 1 0 1 0.0	75 SO	-lute:	CoH	14:	0.223 (mol)		
2. 22 57 57 57 57 57 57 57 57 57 57 57 57 57		0 1365	0 9996	170 1	1.001		07.0		1046 0	3000	73, 8 0 0 0 0	CCD -	27 8.	88 430	0.1	523 0.95	193 5v	1.0 1.02	20		Ċ					
28 26.1	1 439.2	0.1370	0. 9995	172.5	1.065	28 2	0.13	0 8.661	1845 0	7666		050	28 9.	19 43.	1.9 0.1	518 0.95	192 5(6.0 1.02		'nuavi	10		106.1	1100		
29 26.6	3 444.3	3 0.1375	0. 9995	174.8	1.068	29 21	0.61 4	144.8 0	.1845 0.	1 1666	00.2	061	29 9.	54 44	0.3 0.1:	513 0.95	191 Si	8.2 1.02	29							- 1
30 27.1	0 449.2	2 0.1381	0.9994	177.0	1.070	30 2	1.14 4	150.4 0.	.1845 0.	. 9992	102.6 1.	063	30	94 44	5.5 0.1	508 0.99	986 68	0.8 1.0	31	-	۴	:	:	5411		
31 27.5	9 454.0	3 0.1387	0.9993	179.1	1.072	31 2	1.58 4	155.0 0.	.1845 0.	1666 .	104.6 1.	066	31 IO.		0.1	505 0.95 205 0.95		2.5 1.00	55	-	-	<	۲ ¹	12		
0.82 Z8.0	100	1011394	2666.0	180.9	1.075	5 5 F	2.04	459.8 0	.1846 0	0666	106.6 1.	068	32 10.	191 - 30		100 0 00V	001	4.4 7.1 0.1	5 2	. bar	Х	1	1	bar	'	
n 07 07 07	1 160	10110	0.9990	104 5	1.001	2 V 2 V 2 V	80.7	0 0.001	.1849 U	9988	108.9	1/0	34 11.	17 46	5.2 0.1	197 0 90 V	59 59		ן א 3							- 1
35 29.4	5 474 3	3 0.1417	0.9988	185.9	1 083	4 K	- 20	0 7.20#	1854 0	1066	10.4	. 920	35 11.	50 471	0.1	495 0.95	12 080	0.4 1.0	1	1.05	459.7	0.0988	8 0.9894	10.3	1.000	
96.95	479 5	5 0.1427	0.9987	187 3	1 086	ہ ہ ج	- 78 E	178.9	1856 0	Napp		010	36 11.	80 474	1.6 0.1	493 0.95	77 72	2.3 1.00	39 2	1.12	465.3	0.0987	0.9881	11.0	1.001	
37 30.3	484.0	0.1435	0. 9985	188.4	1.089	32	4.33	184.1 0.	.1860 0.	6866	12.21	080	37 12.	17 48(0.3 0.1	492 0.95	17 4 74	4.4 1.04		1.21	470.4	0.0985	0.9870	11.9	1.001	
38 30.8	489.0	0.1444	0.9983	189.7	1.092	38	1.79 4	189, 1 0.	1865 0.	0866	17.3	180	38 12.	48 48	1.8 0.1	491 0.95	171 71	5.3 1.04	13 14	ы. 1.9	4.0.4	0.0984	0.9859	12.7	1.001	
39 31.2	9 494.3	3 0.1455	0.9981	190.8	1.096	33	5, 28 4	194.3 0.	.1870 0.	9978	19.0	088	39 12.	79 48	9.5 0.1	491 0.95	168 71	8.1 1.04	15 7	1.35	480.3	0.0982	0.9848	13.6	1.002	
40 31.7	5 499.5	5 0.1466	0.9979	191.6	1.100	40 2	5.70 4	198.7 0.	.1875 0.	9975 1	20.4 1.	160	40 13.	11 494	1.2 0.1	490 0.95	N65 75	9.9 1.04	10	- 1- 1 -	180.4	02000	0.9839.0	0 L	1.002	
41 32 1	5 503.7	7 0.1475	0. 9978	192.3	1.103	41 20	6.12 5	503.1 0.	.1880 0.	1 E799.	21.7 1.	095	41 13.	47 49	9.5 0.1	491 0.95)61 8 ;	2.0 1.04	19 19	· · ·	1.064	5/60 0 0	0.9823	C.CI	1.003	
42 32.5	4 508.C	0.1485	0. 9976	192.8	1.107	4 2 2t	6.58 5	508.0 0.	.1887 0.	11799.	123.1 1.	, 660	42 13.	83 50	1.7 0.1	491 0.95	357 8:	3.9 1.05	51	1.2	5005	7160.0	0. 9700	0.01	1.000	
43 32.9	2 512.3	3 0.1495	0.9974	193.3	1.110	43 2	7, 14 5	513.7 0.	. 1895 0	. 9967	124.7 1.	103	43 14.	15 50	9.4 0.1	493 0.95	53	5.6 1.0	. 01 01	1 94	202	0.0979	0. 0. 9787	18 9	1 005	
													44 14.	46 51.	3.9 0.1	494 0.9	148 8	7.2 1.0	∷ ≊I	2.06	510.4	0.0972	0.9769	20.1	1.005	
																			12	2.19	515.5	0.0970	0.9754	21.3	1.006	
																			13	2.33	520.5	0.0969	0.9740	22.6	1.007	
																			14	2.46	525.0	0.0967	0.9727	23.9	1.007	
																			J							į

																			Je	oui	rn	al	of	Ċ	he	m	ice	ıl	an	ıd	E	ng	ine	er	inį	g l	Da	ta,	, V	ol.	3	9 , .	No	1. 4	1, 1	199) 4	6	61
			Pntr	1	766.0	0. 997 0. 998	0. 998	0.998	. 998 . 998	0.998	966	. 999	0.999). 999 1 999	. 000	000 .1	000	100	100.														Pntr	I	200 0	799 0	0. 997	0.997	0. 998 0. 998	0.998	0.998	0. 770 0. 998	0.999	0. 999					
	~	-	H ^{PS} 12	bar	1.3	4.0	1.6	1.7	 	2.0		6 6 1 7	3.1		່ ເຕັ	4.2	4.6	4 v 5 (*	5.7										_			5d	H_12	bаг	4	, c	1.0	1.1	1.5	1.6	1.6	- 8-1	1.9	2.0					
	18 (mol	65 (mol	, -	(_	9915	9904 9892	0886	9864 0051	9835	9818 0eno	9787	9769	9750	9729	9690	9671	9651	9631 9611	9590										77 (mol	06 (mol	i		ا ً <mark>ہ</mark>	I	0615	0584	9556	9524	9495 9463	9436	9406 9764	9357	9334	9313					
	0.1	1.6			642 0.	40 0.0	38	37 0.9	5 C 5 C 5 C	32 0.0		26 0.9	24 0.9	22 0.9	17 0	15 0.9	12 0.5		50										0.0	1.5			-		0.00	#04 162 0	461 0.	459 O.	157 U.	453 0.	451 O.	146 0.	143 0.	140 O.					
	H110H:	6H34:	×	I 	6 0.06	900 000 900	6 0.0	20.06	9 0 0 0 7 0	5 0.06		20.0	7 0.06	- 1 - 0 - 0 - 0	2 0.06	9 0.06	0.00	0000	2 0.06										HOE HIS	6H34:			×``	1			0.0	10.0	0 0 0 0	8 0.0	00 00 80	50 50 9	40.0	7 0.0					
	3	ü	-	×	421.	7 431.	9 435.	441.	1 451.	456.	465.	8 470.	475.	0 481. ABK	491.0	495.	201.0	511.0	516.									÷	ð	ü			-	×	0 463	4 467	17 472.	0 477.	J 481.	1 491.	5 496. 0 501	6 506.	2 511.	9 516.					
ble A3	olute;	olvent;	م د	bar	0.3	5 0 0 0	0.4		÷ 10 5 0	0.5		0.0	2.0		5 5 5 6 7 6	56 °O	8 		1.3									able AJ	olute;	olvent;			- ⊑	r. bar		10.0	3 0.3	4.00	0 0 0 0	7 0.5	5 0 0 0 8 0	0.0	1 0.7	2 0.7					
Ta	S	ŝ	2 	2	- '	Ne					, 01	11	12		15	16	17	81 61 	50			_				.1	ŀ	-	Ŵ	ŭ		1	Ē	c	1			• -		•		1	÷ ;	-1					
			Pntr	'	366.0	866.0	366.0	666 0	0.999	666.0	0.999	1.000	1.000	1.000	1.001	1.001	56	1.002	1.002	1.002	1.003	1.003	1.004	1.005	1.005	1.006							Pntr	•	000	0.999	0.999	1.000	1.000	1.000	1.000	1.001	1.001	1.002	1.003	1.004	1,004	1,005	1.006
	(I o	01)	H ^{PS} 12	bar	4.7	5.0	9.4	7.8	ຜ່ອ	10.0	10.9	12.6	13.6	14.3	16.4	17.5	19.4	20.9	22.1	23.4	26.1	27.8	29.3	32.4	34.3	36.3		:	0I)	01)			H73	bar		1.6	9.1	9.7	11.3	12.1	12.1	13.5	15.1 16.0	17.1	19.4	21.6	23.1	26.1	27.8
	0.151 (n	1.872 (m	۲ <mark>،</mark>	1	0. 9993 0. 9992	0.9990	0.9989	0.9984	0.9981	0.9974	0.9970	0.9961	0.9956	0.9951	0. 9937	0.9930	0.9921	0. 9902	0. 9892	0.9882	0.9860	0.9846	0.9834	0.9809	0.9794	0. 9778			D. 205 (m	2.058 (m			y,	ı	10000	0. 9934	0.9921	0.9912	0.9895	0.9885	0.9847	0.9839	0.9834 0.9819	0.9807	0.9798 0.9789	0. 9773	0.9762	0.9735	0.9722
	H:		×「	Т	0.0726	0.0722	0.0720	0.0716	0.0714	0.0710	0.0708	0.0704	0.0701	0.0700	0.0695	0.0693	0.0691 0.0689	0.0687	0.0685	0.0682	0.0678	0.0676	0.0674	0.0669	0.0667	0.0665			÷				×	T	0.0070	0.0879	0.0880	0.0879	0.0876	0.0875	0.0876 0.0876	0.0874	0. 0871 0. 0870	0.0868	0.0866 0.0865	0.0863	0. 0861 0. 0859	0.0858	0.0857
	C3H7O	C16H3	н	¥	372.1	382.2	386.9 392.7	396.9	402.0	411.9	417.3	426.9	431.9	435.8	446.3	451.1	455.8	466.3	471.2	476.1	485.6	491.2	495.9	505.3	510.6	516.1		1	CeH90	C16H34			г	¥	1 424	1.86	443.8	448.8	458.2	463.0	1.12.7	477.9	182.6 187.7	192.6	196.9 500.5	507.3	512.2 (516.8 (521.6	526.7
le A28.	ute;	vent;	-	bar	0.38 0.38	0.43	0.52	0.56	0.62	0.72	0.79	0. 00 10 10 10	0.97	1.02	1.17	1.24	9 e - 1	1.48	1.56	1.74	1.84	1.95	5.02 1:02	2, 27	2.40	2.54		E 173.	ite;	ent;			₽	bar	60 0	0.82	0.82	0 88 6	1.02	1.09	1.10	1.22	1.37	1.55	1.67	1.96	2. 10 2. 25	2.37	2.54
Tab	sol	sol	Iun	2	- ~	i m	4 10	o vo	- 8	6	9:	12	13 13	4 <u>1</u>	16	17	2 5	20	21	3 2	24	52	26 77	58	29	8	ŀ	f die f	solu	solv		1	гuп	hr.	-	- 0	e .	4 V	o vo	7	0 0	10	12	13	14	16	17	19	8
												Phtr		·	0.999	0.999	1 000	1.000	1.000	1.000	1.000	1.001	1.001	1.001	1.002	1.002	1.002	1.002	1.003	1.003	1.003	1.004	1.004	1.005	1.005	1.006	1.007	1.007											
								1	: =	1		HPS 2		DAL	10.8	11.8	13.7	14.9	16.0	10.7	19.8	21.1	22.5	23.7	26.5	27.9	29.4	30.7	32.25	35.1	36.9	38.9	42.3	44.3	46.3	50.3	52.6	54.8											
								129 (mo	864 (mo	DIII 1 100 .		۲, ۲	ʻ	, 	0. 9996	0.9995	0.9994	0. 9992	0.9990	0.9988 0.9986	0. 9983	0.9981	0. 9977	0.9973 1.0060	0.9965	0.9960	0.9954	0.9949	0,994.5	0. 9928	0.9919	0.9909	0. 9891	0.9879	0. 9868 0 9854	0. 9843	0.9829	0.9816											
								c	- ·	•		×		,	. 0605	. 0603	01697	. 0595	. 0592	0589	.0584	. 0581	. 0578	. 0576	.0572	. 0569	. 0567	. 0565	1920.	. 0559	.0557	. 0555	0551	0549	0547	0543	0542	0540											
								-HOH-	CieHae:		ļ	г	>	4	73.1 0	77.4 0	81. / U	91.9 0	96.6 0	02.2 0 8 70	12.4 0	17.0 0	22.4 0	27.2 0	37.0 0	11.6 0	17.0 0	51.0 0	0 5 15	55.6 0	70.9 0	76.4 0	35.4 0	0.6 0	95.6 01.1 0	5.4 0	0.6 0	5.5 0											
							A27.	<u>ح</u>		-		Ь			. 66 3	. 72	5 C 8 -	6 6 6 7 6	. 96 J	- 04 11	. 18	. 25 4	.32 4	66	- 22 - 22	.62 4	.71	. 78 19	98 - 1 6	- 62 - 62	.12 4	5 S	367 - 167 -	.52 4	29. 27. 49.	. 85 50	.97 51	. 09	I.										
							Table	solute	solver	124100		гun	nr.		1	~ ~	າ ເ	, 0 , 0	9	. α	• •	10 1	11	22 21	14	15 1	16	17	2 0 2 0	20 2	21 2	22	24 2	25 2	07 C	28 2	29 2	8											
												Pntr		, 	1.000	000	000	. 002	1. 002	. 003	. 003	. 004	. 004	1. 004	. 005	. 005	. 006	1.006	200	.007	1.008	808	600.	. 010	010	. 010	. 011	. 011											
								_		_		H ^{PS}		IPO	15.3	15.2	8.CI	26.0	30.1	32.0	5 6 5 6	37.6	39.7	41.9	46.0	48.2	50.1	52.1	54.4	28.0	59.6	61.5	65.3	66.7	67.4 68 1	69.1	70.0	71.3											
								(W) 141	10m) #01	TOW) 040		۲,	1	1	. 0000	6666 ·	9999 9998	7997	. 9995	. 999 4 9992	. 9992	0666 .	8866	. 9986	. 9981	8796	. 9975	. 9972	1966 -	. 9959	9954	. 9948	. 9934	. 9928	9921	9066	7686	9889											
								c		j		×	4		0675 1	0676 0	0 6640	0653 0	0647 0	0644 0	0638 0	0636 0	0634 0	0631 0	0627 0	0625 0	0623 0	0622 0		0618 0	0618 0	0618 0	0617 0	0617 0	0618 0	0621 0	0622 0	0622 0											
								HOr	CicHae-		l	Т	-		6.1 0.	1.3 0.	0.0	3.8 0.	5.1 0.0	0.7 7 0.	0.4 0.	5.1 0.4	0.6 0.1	5.7 0.	5.5 O.1	0.6 0.1	5.5 0.1	0.2		1.5 O.C	9.4 0.1	4.4	1.6 0.t	8.8 0.	2.9 0.5	0.0	4.9 0.1	9.2 0											
							126.	Ę		,		۵.	ر - ا		.05 34	05 35	40 30 190	74 38	00 39	12 40	96 114 98	46 41:	59 42	.72 42 84 42		11 44	23 44	35 45	CP 45.	25 1 6	83 46	94 47	19 48	29 48	404 404 404	48 500	55 50	64 50											
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662	Journal of Chemical and Engi	neeri	ng .	Da	ta,	Ve	ol.	39 ,	, N	o. 4	4, 1	99	4									
	Patr		1.031	1.033	1.034 1.035	1.035	1.036 1.037	1.038	1.039 1.041	1.042	1.044	1.045 1.046	1.048	1.050	1.052 1.053	1.054	1.058	1.059	1.061 1.063	1.065	1.067 1.069	

	H ^{PS} 12 bar	91.5 1 93.7 1 96.1 1 98.5 1 101.5 1 104.0 1 104.0 1	109.5 112.2 114.9 117.9 120.7 123.5	125.9 129.1 131.1 133.7	1353.5 1463.1 140.7 147.4 147.4 157.7 155.5 151.5 157.7 157.7 151.5 161.6
58 (mol 21 (mol	- <mark> </mark>	8666 6666 6666 0000	9998 9997 9995 9995	9992 9990 9988 9986	9983 9976 9972 9954 9928 9928 9918 9918 9918 9918
0.4	-1	335 1. 329 0. 316 0. 303 0. 298 0.	292 0. 286 0. 281 0. 271 0. 271 0. 271 0.	264 0. 261 0. 259 0. 257 0.	22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
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Ü CSHP CSHP	× +	381. 385. <td> 413. 418. 423. 423. 423. 433. </td> <td>443. 453. 453.</td> <td>462: 462: 478: 478: 478: 487: 487: 487: 487: 487: 487: 487: 487: 487: 487: 487: 493: 487: 493: 487: 493: 494: 495: 495: 495: 495: 495: 497:</td>	 413. 418. 423. 423. 423. 433. 	443. 453. 453.	462: 462: 478: 478: 478: 487: 487: 487: 487: 487: 487: 487: 487: 487: 487: 487: 493: 487: 493: 487: 493: 494: 495: 495: 495: 495: 495: 497:
Je A 36 lute; ivent;	par	13.29 13.82 13.82 14.10 14.14 14.74 15.04	15.39 15.71 16.00 16.38 16.71 17.09	17. 37 17. 77 17. 99 18. 35	22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Tal		-004000	8 0 1 2 2 0 8 8	14 15 16 17	8 3 3 3 3 3 3 3 3 9 8 9
	Pntr -	1.062 1.064 1.065 1.066 1.068 1.068 1.069	1.072 1.074 1.076 1.077 1.077 1.079	1.083 1.085 1.087 1.087	1:091 1:093 1:098 1:098 1:108 1:110 1:111 1:111 1:1120 1:123
	H ^{PS} 12 bar	710.8 713.3 713.1 713.1 710.4 710.5 712.4	714.1 718.4 718.6 719.6 717.6	712.9 709.5 708.0 707.5	706. 1 702. 7 702. 7 702. 3 696. 9 664. 3 664. 3 664. 3 664. 3 664. 3
26 (mol	5		66666 0000	7666 7666 7666	9995 9995 9995 9989 9985 9976 9972
1. 6. 1. 6.		66 1- 66 1- 175 1- 182 1- 193 1- 193 1- 1-	001 1. 005 0. 015 0. 022 0.	551 0.0	5552 0.0 5552 0.0 55552 0.0 5552 0.0 55
H330H:	× ⁻ +	2 0.04 2 0.04	2000000 000000 000000	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
H2: C1e	× ×	372. 376. 385. 385. 391. 395.	404. 410. 415. 425.	435. 440. 450.	454. 459. 459. 459. 474. 485.
Je A 35 (ute; (vent;	bar P	34.82 35.24 35.67 35.67 36.12 36.61 37.05	39.52 39.52 39.52 39.52	40.95 41.44 41.89 42.38	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Tat so1			805155	16 15 4	183838838838283838383838383838
	Pntr	1.036 1.037 1.038 1.038 1.038 1.040 1.040	1.043 1.044 1.045 1.045 1.047 1.048	1. 050 1. 051 1. 053 1. 053	1: 058 1: 059 1: 061 1: 063 1: 063 1: 074 1: 074 1: 074
(1)	H ^{PS} 12 bar	141.6 141.6 145.3 149.2 153.4 153.4 155.8 155.3 159.3 159.3	164.9 164.9 171.6 174.5 177.2	180.8 180.8 184.0 188.1 190.9	193. 9 196. 7 196. 7 202. 0 208. 6 210. 9 212. 6 213. 1 213. 1 221. 9 224. 1
529 (mc 621 (mc	v 1	0000 0000 0000	9999 9998 9998 9997 997), 9995), 9995), 9993), 9993	5 9995 5 9988 5 9989 5 9973 5 9973 5 9953 5 9955 5 99555 5 995555 5 995555 5 995555 5 9955555 5 9955555555
о́ г 	x"	1215 1 1207 1 1198 1 1191 1 1187 0 1186 0 1186 0	11181 11811 111811	1189 1187 1184 1184 1184	
:: 16Н330H		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
. 34. 		2 2 8 3 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4 3 3 4		338 433 25 443 61 450	200 200 200 200 200 200 200 200
äb le A olute;	d n i	2 19. 0 1 18. 19. 0 19. 19. 0 19. 19. 0 19. 19. 0 19.	8 5 5 5 5 7 5 8 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	15 23. 24 23.	8 2 2 3 7 3 7 3 2 3 5 8 3 8 8 8 8 9 9 9 7 7 7 7 8 9 9 9 9 9 9 9 9
ntr 11 11 11 11 11 11 11 11 11 11 11 11 11	- 700 008 008 1 2 800 800	0009 011 012 013 013 013 015		ntr	064 065 065 072 072 072 072 072 072 072 072 072 072
Part 1	11.2 1. 33.5 1. 88.3 1.	1		PS P	88.8 99.9 99.9 99.9 99.9 90.9
9982 6992 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	962 957 946 800 946	940 929 10 915 11 906 11 887 11 887 11 879 11	3 (mol) (mol)		000 000
× 100 000 000 000 000 000 000 000 000 00	226 0.9 224 0.9 223 0.9	220 0.5 208 0.5 208 0.5 208 0.5 208 0.5 208 0.9 209 0.9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.57	× -	07 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 1 0 0 1 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0
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T T T T T T T T T T T T T T T T T T T	11 467. 52 472. 55 477. 78 482.	34 487 35 491. 35 496. 31 506. 31 506. 31 506. 32 511. 36 521. 35 521.	3. 0. 2.	н м	372 372 36 372 376 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 385 410 385 410 385 410 386 410 387 410 387 410 386 410 387 410 386 410 387 410 388 410 388 410 388 410 388 410 388 410 388 410 388
2 1 0 0 8 2 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 2 2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 4 4 4 4 4 4 4 4 4 4 4 4	able A 3 olute; olvent;	un F. bar	1 1 2 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
			ι Η ο ŏ	LĊ	

0.145 (mol) 1.952 (mol)

Table A3	7.					Tabl	; A38.						Tabl	e A40.						Table	A41.					
solute;	C3H8:	0	175 (mo)	2		solu	;e;	C5H12		0.090 (m	01)		solu	te;	CH∋OH:	Ū	0.158 (mc	(]		solut	e.	C2H5OH:	0	.160 (mol	~	
solvent;	C16H	1 :HOEEI	.621 (mol	9		solv	ent;	C16H3	30H:	1.922 (m	ol)		solv	ent;	C16H33	CH:	l.621 (mo	(1		solve	int;	СтыНаз(CH: 1.	.625 (mol	~	
run P Bar	+ ¥	× -	, v	H ^{PS} 12 bar	, P	n. ur	P bar	 ⊢ ×	×	Y1	H ^{PS} 12 bar	- Pntr	E 문	P red	⊢ ⊾	×"	y,	H ^{PS} 12	Putr	n	P 4		×" 1	× -	H ^{PS} 12 bar	Pntr
	4							:						Dar	4	,	,	Dar	,			4				
1 3.2	3 372.2 1 376.3	0.0708	0.9999	44.0	1.007	- 2	0, 30 94	380.7 385.2	0.0430 0.0428	0. 9991 0. 9990	7.9	0. 997 0. 997	- 0	0.35	370.9 (0.0860	0. 9996	4.0	0.999	- ~	0.31	381.2 (0.0875 (0.0872)	0.9992	3.5 4.0	0. 998 0. 998
3.3	3 380.5	0.0707	0. 9999	45.4	1.007	n	0. 38	390.8	0.0426	0.9987	8.9	0.998	1 m	0.46	381.9	0.0852	0. 9994	5.4 0	0. 999	n U	0.41	392.1 0	0.0868	0. 9988	4.7	0.998
4 3.4	3 384.8	0.0702	0.9999	47.2	1.007	4 u	0.42	396.1	0.0424	0.9984	9.8 10.5	0.998	4	0.54	387.3 (0.0847	0.9993	6.3	0.999	4	0.46	396.8	0.0864	0.9986	с. •	0, 999
9 9 9 9 9 9 9	7 395 0	0.0691	0.9998 0.9998	51.3	1.008	n u	0.48	406.3	0.0421	0.9975	11.3	0.998	un v	0.61	392.0	0.0842	0.9992	7.1	0.999	un v	0.53	402.1 (0.0860	0.9980	1.0	0. 999
7 3.7	9 400.1	0.0687	0. 9997	53.2	1.008	-	0.52	410.6	0.0420	0.9971	12.1	0.998	• ~	0.75	401.2 (0,0833	0.9988		0. 999	• ~	0.66	411.9 (0.0852	0. 9976	7.7	0.999
8 3.9	1 405.0	0.0682	0. 9996	55.3	1.009	80	0.55	416.6	0.0419	0.9963	13.1	0.998	. 80	0.84	406.7	0.0827	0. 9986	10.1	1.000	• 00	0.73	416.6	0.0848	0. 9973	8.5	0.999
9.4.0	5 410.0	0.0675	0. 9996	57.9	1.009	6 6	0.59	421.1	0.0417	0.9956	14.0	0.998	6	0.94	112.1	0.0821	0. 9983	11.3	1.000	6	0.81	422.2	0.0843	0.9967	9.5	1.000
10 4.2	4 415.3	0.0666	0.9994 0.9993	61.3	1.010	2:	0.67	431.2	0.0414	0.9936	14.0	0.999	9:	1.04	417.2 (0.0815	0.9980	12.6	1.000	9:	0, 90	427.6 (0838	0.9961 0.9955	11.7	1.000
12 4.5	2 424.6	0.0654	0. 9992	66.6	1.011	12	0.71	435.9	0.0413	0.9925	16.9	0.999	1 2	1.23	426.8 (0.0803	0.9972	15.1	1.001	12	1.07	437.1 (0.0828	0.9948	12.7	1.000
13 4.7	9 430.4	0.0647	0. 9989	69.9	1.011	13	0.74	440.3	0.0412	0. 9912	17.7	0.999	13	1.35	432.1 (0.0797	0. 9967	16.6	1.001	13	1.17	442.3	0.0823	0.9940	14.0	1.000
14 4.8	4 435.4	0.0641	0. 9987	72.6	1.012	14	0.78	446.1	0.0411	0.9891	18.7	0.999	14	1.45	137.0 (0.0791	0.9961	18.0	1.001	14	1.27	447.4 (0.0818	0.9930	15.2	1.001
15 4.9	7 440.0	0.0637	0.9984	5. C	1.012	c1 4	0.84	450.8	0.0408	0.98/6	2.02	1 000	15	1.57	442.1	0.0785	0.9955	19.6	1.001	15	1.37	452.2	0.0813	0.9920	17.0	100-1
16 5.1 17 5.7	1 444./	0.0630	0. 9977 0. 9977	5 . 1 I	1.013	17	0.93	460.3	0.0406	0. 9831	22.2	1.000	17	1.68	146.4 (0.0779	0.9948	21.1	1.002	9 C	1.48	457.3	0803	0. 9895	19.1	1.002
18 5.3	5 454.4	0.0626	0. 9972	82.1	1.013	18	0.97	464.8	0.0405	0.9805	23.1	1.000	18	1.95	157.2 0	0.0765	0.9928	24.9	1.002	18	1.67	466.4 (0.0798	0.9881	20.4	1.002
19 5.4	8 459.2	0.0623	0. 9966	84.4	1.014	19	1.01	469.9	0.0404	0.9771	24.1	1.000	19	2.02	161.9 (0.0759	0.9918	26.6	1.003	19	1.78	471.1	0.0793	0.9864	21.7	1.002
20 5.6	4 464.7	0.0618	0. 9959	87.3	1.014	20	1.06	474.8	0.0403	0.9735	25.2	1.000	20	2.19	166.9	0.0753	0. 9905	28.4	1.003	20	1.91	477.3 (0.0787	0. 9839	23.5	1.002
21 5.7	8 469.8	0.0615	0.9951	89.9	1.015	21	1.11	480.0	0.0401	0.9693	26.6	1.000	21	2.33	472.1 0	0.0747	0.9890	30.3	1.003	21	2.03	482.1 (0.0782	0. 9817	25.0	1.003
22 5.9	4 475.3	0.0611	0.9941	92.8	1.015	22	1.17	484.9	0.0400	0.9648	27.8	1.001	22	2.44	176.3 (0.0742	0.9876	31.9	1.004	22	2.15	487.1 (0.0777	0.9791	26.6	1.003
23 6.0	8 480.2	0.0608	0.9931	95.4	1.016	2 2	1.24	489.0	0.0398	0.9606	C. 67	1.001	53	2.57	181.4 (0.0737	0.9856	33.8	1.004	23	2.26	491.4 (0.0773	0.9767	70.82	1.004
24 6.2	1 4184.9	C090.0	0.9006 0	100 4	1.017	52	1.37	499.8	0.0396	0.9484	32.3	1.001	24	2.71	1.98	0.0731	0.9833	8.8 8.6	1.004	24	5.5	4940.00 501 6 (0.0763	0.96.99	31.3	1.004
26 6.4	9 494.4	0.0600	0.9892	102.8	1.018	5 2	1.44	505.0	0.0394	0.9416	34.0	1.002	3 2	2 86 7 86 7	196.4	CZ 10.0	0. 9784	30.6	- 002	67 97	2.66	506.9 506.9	0.0758	0.9658	33.1	1.005
27 6.6	5 500.0	0.0597	0. 9872	105.5	1.018	27	1.49	509.5	0.0394	0.9341	34.8	1.002	21	3.13	501.9 (0.0716	0. 9751	41.8	1.005	27	2.79	512.0	0.0754	0.9614	34.9	1.005
28 6.7	8 504.3	0.0595	0.9854	107.9	1.019	28	1.58	515.0	0. 0392	0.9256	36.7	1.002	. 28	3.26	506.4 0	0.0711	0.9720	43.6	1.006	28	2.94	516.8	0.0749	0.9568	36.7	1.006
29 6.5 30 7.1	4 509.6 1 514.7	0.0590	0.9804	113.2	1.020	Table	. A39.						R 8	3.56 3.56	516.7 0	0.0702	0.9684 0.9638	45.6 47.8	1.006 1.007							
						solut	ë	Colli 4		0.087 (m	(10									Table	A42.					
						solve	nt;	C16H3.	30H:	1.922 (m	(10									solut		C3H7OH:		10ml) 860	~	
																				solve	nt;	C16H33O	H: 1.	629 (mol	~	
											P5															
						run	-	-	×~	~"	12										٥	F			5411	
						nr.	bar	Ж	ŧ	T	bar	1								E	-	-	~ "	- 	12 12	
						-	10	2 004	0.0419	0 0020	4 L	0 007									oar	×	ŧ	1	bar	1
						0	0. 34	426.0	0.0417	0.9904	8.0	0.997								-	0.00	126.6.0	0542	9896	а 2	800 0
						e -	0.36	431.0	0.0416	0.9884	8.4	0.997								2	0.35	131.5 0	.0540	. 9882	6.4	0. 998
						4 v	وي . 14 م	4.35.9	0.0414	0 9844	1.6	766 .0 0. 997								 ო •	0.38	135.9 0	.0538 0), 9865 . 2011	6.9 9	0.998
						o 0	0.44	444.8	0.0413	0.9821	10.3	0.998								ar ⊮0	.47 47	141.2 0	. 0533 0	. 9819	- 9.8	0. 998 0. 998
						2	0.47	449.3	0.0412	0.9795	11.0	0.998								s	0.51 4	151.7 0	.0531 0	. 9796	9.4	0.999
						x 0	0.50	454.5	0.0412	0.9758	17.6	0.998								~ (0.55	56.3 0	.0529 0	0. 9769	10.2	0.999
						. 5	0.57	465.1	0.0409	0.9675	13.4	0.998									10.0	166.4 0 U	0 4250.0	0.97.34	12.0	9999 C
						11	0.62	470.0	0.0408	0.9633	14.5	0.998								, 5 1	22.0 7.12	172.0 0	.0521 0	0.9658	13.0	0.999
						12	0.64	474.0	0.0407	0.9587	15.0	0.998								11	0.75 4	175.9 0	.0519 0	. 9625	13.9	0. 999
						14	0.75	485.5	0.0405	0.9452	17.3	0.999								212	. 83	81.9 0	.0516 0	1. 9569 1. 9512	15.2	0.999
						15	0.79	489.8	0.0404	0. 9387	18.1	0.999								14	. 95	91.7 0	.0510 0	0.9461	17.4	000.1
						1 I E	0.84	494.6 199 6	0.0402	0.9319	19.2 20.4	0.999								15	1.01	96.7 0	. 0508 0	. 9396	18.6	1.000
						18	0.95	504.6	0.0400	0.9149	21.6	1.000								19	15 5	02.0	. 0505 0	0. 9325 0. 0351	19.9	000
						19	1.02	509.8	0.0399	0.9047	22.7	1.000								18		0 6 01	0.0501	1626.0	21.9	100
						20	1.08	514.9	0.0397	0.8942	24.0	1.000								19	. 31 5	16.8 0	0498 0	. 9073	23.5	1.001

Table A43.					Tabl	e A45.						Table A	7.					Table	A49.				
solute;	C4H9OH:	0.115	(mol)		solu	ite;	C6H13	OH: ().093 (mo.	(1		solute;	ë		0.745 (1	1)		solute	8	12:	0.522	(mol)	
solvent;	Сл 6НээОН	: 1.637	(mol)		solv	ent;	C16H3	:HOE	.621 (mo	1)		solvent;	3	eHse:	0.332 (1	Nol)		solven	ţ.	C28H58:	0. 332	(mol)	
			. P5							s d						PS.				, ,	:	s d ⁿ	Putr
۲ ا	-		¹ 12		run	×	-	×「	>"	H12	Pntr	ي ا ۲	-	×"	×_	¹ 12		un 1	.	- -		.12	
nr. bar	Х	1	bar	ι	nr.	bar	×	I	ł	bar	ı	nr. baı	X	1	I	bar	ı	а	ar	К –	1	bar	'
1 0.31	441.7 0.(0.97	89 4.8	966.0	-	0.31	480.6	0.0526	0.8945	5.3	0. 997	1 30.	4 423.	9 0.097	1 1.0000	308.8	1.083	1 18	.67 39	7.9 0.11	48 1.000	0 140.4	1.046
2 0.35	445.9 0.(0.97 723 0.97	71 5.3	0.998	20	0.34	486.1	0.0525	0.8809	5.6	0.997	2 31.1	7 428.	9 0.092	7 1.0000	311.1	1.085	2 18	.88 40 74 40	21.0 2.50 11.0 8 80	246 1.000	0 144.5	1.048
4 0.42	456.9 0.0	1629 0.96	3.0 96 6.5	0.998	n 4	14.0	490.5	0.0524	0.8/11	9.1 9.2	0.997	9.17. 17.17.	12 433.	5 0.098 9 0.088	4 1.0000 e 1.0000	313.2	1.087	4 19	43 41	15.9 0.12	242 1.000	0 147.7	1.049
5 0.47	462.0 0.0)627 0.96	59 7.2	0.998	۴uo	0.44	499.5	0.0522	0.8511	7.1	0.998		444	9 0.094 0 0.094	7 1.0000	315.9	1.091	5 19	. 69 42	20.9 0.12	34 1.000	0 150.2	1.050
6 0.51	467.0 0.0	0625 0.96	20 7.8	0.998	9	0.49	506.1	0.0520	0.8340	7.9	0. 998	6 32.7	1 448.	7 0.087	4 1.0000	317.1	1.093	9 19	.93 42	22.6 0.12 0.02	232 1.000	0 152.0	1.051
0.56	4/1.6 0.0	1622 0.95 1620 0.95	80 8.5 25 0.2	0.998	r 0	0.54	510.6	0.0518	0.8228	80 0 00 0	0.998	7 32.8	12 455.	2 0.108	6 1.0000	318.8	1.095	- x	202	32.7 0.13	0001 000	0 156.2	1.054
99 0.66	481.7 0.0	1618 0.94	71 10.0	666 0	•	60.0	0.010	0100.0	0.8103	2.6	0. 798	2.5 2.5 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6	14 46U	260.0 /	8 1.0000	321.4	1.100	6 50	.57 44	10.4 0.12	296 1.000	0 158.6	1.055
10 0.71	487.1 0.()616 0.94⊌	06 10.8	666 0								10 34	5 468.	7 0.088	6 1.0000	322.3	1.101	10 20	. 99 44	15.0 0.1	181 1.000	0 160.9	1.056
11 0.77	491.8 0.0	0.93 0.93	46 11.6	0, 999								11 34.	13 473.	8 0.093	5 1.0000	323.5	1.103	11 21	. 06 8	50.2 0.1 0.1 0.1	293 1.000	0 163.3	1.050
12 0.82	502 - 0.0	1611 0.92 1609 0.914	8.21 12.4 13.4	0.000								12 34.	2 479.	0 0.098	6 1.0000	325.3	1.106	13 21	. 1 7 86	59.4 0.1	101 1.000	0 167.6	1.060
14 0.96	506.9 0.0	16.06 0.91	11 14.3	000								13.35	1984 0	0.094	7 1 0000	328.0	1.108	14 21	. 98	55.1 0.1	197 1.000	0 170.0	1.062
15 1.04	511.8 0.(0. 90, 90,	25 15.3	1.000								15 35.	5 495.	7 0.098	0 1.0000	329.2	1.114	15 22	. 34 4	70.1 0.1	139 1.000	0 172.5	1.063
16 1.11	516.3 0.0	0.89	40 16.2	1.000								16 36.	30 S00.	1 0.096	4 1.0000	330.3	1.117	16	54 40	75.5 0.1	179 1.000	0 175.5	1.065
					i i i i							17 36.	505.	1 0.104	5 1.0000	331.7	1.119	18	287 12 48 48	35.3 0.1	133 1.000	0 180.2	1.068
					TopI	C 740.						18 37.4	802 00	7 0,110	2 I.UUUU	0.766	1.121	19	3.37	90.3 0.1	133 1.000	0 183.2	1.070
					solu	te;	H20:	5	.109 (mol	•		- 16 02	520	0 102	1 1 0000	335.7	1.128	20	3.44 49	94.7 0.1	211 1.000	0 185.2	1.071
					solv	ent;	C16H3.	30H: 1	.617 (mol	-								21 2:	3.55 4	98.4 0.1	250 1.000	0 187.5	1.072
																		22	3.82	04.2 0.1	265 1.000	0 190.6	1.074
																		22	6. 1	1.0 2.60	100 I. 001	105.0	1 078
					Lun	P.	т	×	۲ ₁	H ⁷⁵	Pntr							52 52 53	1.95 1.95	19.4 0.1	078 1.000	0 199.4	1.080
					п.	;	>	'	'	1													
						DAI	4	·	1	IPO	,	Table A4	8					Table	450				
					-	0.34	373.0	0.0604	0. 9995	5.7	0.999		;		1 200 0								
					5	0.38	377.2	0.0601	0.9995	6.4	0. 999	solute;	H2:			(10		solute	C2	H6:	0.741	(mol)	
					~ -	0.45	382.1 387_1	0.0596	0.9994 0.9994	7.5 8 6	0.999	solvent;	8	BH50:	0.332 (m	01)		solven	- 1	C28H58:	0. 332	(mol)	
					ŝ	0.58	392.2	0.0586	0. 9991	9.9	0. 999									ĺ			
					Ŷ	0.65	396.3	0.0581	0.9990	11.1	0. 999	д	T	×	>	HPS	Pntr		٥	T v		sан	Putr
KEV STOPT		~			- 0	0. /4	401.6	0.05/5	0.9988	12.7	1.000	run 22		-	-1	12		E I	.	;" .		12	
solute;	CSH110H	. n. IU	(10)		• •	0.92	411.9	0.0563	0. 9983	16.2	1.000	m. bar	X	I	ı	bar	i	р Э	аг	ı ۲	ł	bar	ı
solvent;	C16H3301	H: 1.62	1 (mol)		10	1.00	416.5	0.0558	0. 9980	17.7	1.000	1 41 4	914	2960 0 2	1 0000	425.9	1 102		5		000 - 10	1	100
					=:	1.11	421.8	0.0551	0.9976	19.9	1.000	2 42.5	3 429.	6 0.087	1.0000	439.1	1.106	2 24	98 42	8.8 0.28	84 1.000	2.67 0	1.078
£	۲	;	54H	Putr	1 1	3 6 1	4.32.0	0.0538	0.9966	24.1	1.001	3 42.9	5 434.	2 0.0883	1.0000	444.3	1.108	3 25	.30 43	3.9 0.28	95 1.000	0 76.9	1.079
run r	-	~ < -)	1 12		14	1.42	437.2	0.0532	0.9960	26.4	1.001	4 43.5	3 439.	4 0.0835	1.0000	448.1	1.111	4 25	.67 44	0.1 0.29	15 1.000	77.5	1.082
nr. bar	×	1	bar	1	15	1.53	442.2	0.0525	0. 9953	28.8	1.001	6 44.3	8 449.	1 0.0893	1.0000	458.9	1.115	5 26 7 26	00 44 0C	2.3 0.28	16 1.000 97 1 000	2011 2012	1.083
					- 16	1.64	447.0	0.0520	0.9945	31.0	1.001	7 44.8	8 454.	2 0.0880	1.0000	464.7	1.118	7 26	64 45	5.2 0.29	38 1.000	0.01 0	1.087
1 0.31	450.5 0.	0587 0.9	686 y.	1 0.99/	11/	د . I ۲	451.9	0.0503	0.9936	9.75 9.75	1.001	8 45.2	9 458.	4 0.0877	1.0000	470.2	1.120	8 27	01 46	0.1 0.29	24 1.000	80.3	1.089
2 0.34 20 1.34	461 3 0	0.583 0.9	6. 293 6.	2 0,998	19	2.00	462.4	0.0500	0.9913	39.1 39.1	1.002	9 45.8	6 464.	0 0.0862	1.0000	479.2	1.123	9 27	41 46	4.6 0.28	88 1.000	0 81.2	1.091
4 0.41	465.6 0.	0581 0.9	553 6.	7 0.998	20	2.11	467.1	0.0495	0.9900	41.6	1.002	10 46.3 11 46 7	9 468. 7 473	6 0.0811 5 0 0860	1.0000	483.3	1.126	10 27	. 76 46	8.8 0.28	63 1.000	81.7	1.093
5 0.45	470.6 0.	0579 0.9	502 7.	4 0.998	21	2.22	471.4	0.0490	0.9886	44.2	1.002	12 47.2	7 478.	7 0.0864	1.0000	497.3	1.131	12 11 28	26 47	9.0 87079	32 1 000	02.J	1 097
6 0.50	476.3 0.	0577 0.9	436 8.	1 0.998 7 0.998	22	2.33	476.4	0.0484	0.9869	46.9	1.002	13 47.7	6 483.	4 0.0842	1.0000	504.2	1.134	13 28	64 48	3.8 0.29	19 1.000	83.9	1.100
9C.0 7	480.5 0	2.0 0/c0.	371 9.	4 0.998	542	2.59	487.1	0.0473	0.9823	53.1	1.003	14 48.2	3 488.	1 0.0834	1.0000	507.6	1.137	14 28	88 48	8.8 0.29	54 1.000	0 84.5	1.102
9 0.64	490.7 0.	0571 0.9	238 10.	2 0.999	55	2.70	491.6	0.0469	0.9800	55.8	1.003	15 48.6 16 49 0	6 492. 7 497	9 0.0851	1.0000	515.4	1.140	15 29	27 49	3.7 0.29	34 1.000	0 85.3	1.105
10 0.65	495.5 0	.0569 0.9	161 10.	9 0.999	26 27	2.82	496.3	0.0464	0.9773	58.4	1.003	17 49.6	2 502.	6 0.0836	1.0000	528.5	1.146	10 29 17 29	86 50 50	5.1 0.30	24 1.000 04 1.000	0.00 8.98	1. 110
11 0.74	500.6 U	.0567 U.S	072 11.	5 0.999	280	8 8 1 6	201. A	0.0454	0.9701	61.8 65.0	1. UU4	18 50.0	7 507.	1 0.0829	1.0000	532.6	1.149	18 30	24 50	9.2 0.29	67 1.000	87.7	1.113
12 0.86	510.5 0.	0563 0.8	876 13.	4 0.999	5 6	3.21	511.5	0.0450	0. 9662	67.8	1.004	19 50.5	3 511. 2 516	8 0.0822 9 0.0925	1.0000	540.1	1.152	19 30	38 51	3.7 0.30	28 1.000	88.3	1.115
14 0.95	515.9 0	.0561 0.8	755 14.	3 1.000	8	3. 34	516.3	0.0446	0.9619	70.8	1.005	2.1.		0 0.000	1	>		7 7 7	10 10	8.6 U.Ju	42 1.000	1 87.1	1.118

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.1	56 (mol)		Table A5. solute;	3. CeH14		.070 (mol)		Tab) solv	le A55. ute; (2HSOH:	0.132	(mol)		Table	A57.	AHaOH-	0 070	(lo	
$ \begin{array}{ $	5				-110	c i	(10-) 666		1		Conflee				SULUC		UDAUN.			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	(mol)		solvent;	C28Ht	:e:	(10m) 288		sol ^y	vent;	C28H58:	0. 337	(mol)		solven	ں ت	C28H58:	0.352 (i	mol)	
$ \begin{array}{ $	> 1	H ^{PS} 12 bar	Pntr	run P nr. bar	н ¥	×	, 1 1 1	H ^{PS} Put		۵. <u> </u>		~ ^r	H ^{ES} 12	Pntr	H L L L L L L L L L L L L L L L L L L L		×"	, '	H ^{PS} H12 bar	Pntr
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				1 0 2	A CTF 8	0 1590	0000	1 8 0 9	 2	bar	_ _	1	bar	·	j					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	88	00 32.5	1.012	2 0.3	2 378.8	0.1575	1. 0000	2.0 0.9	1 16	2.68	24.7 0.1	683 1.000	0 15.4	1.005	1	.83 42:	3.6 0.18(0000 1.0000	4.5	0.999
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	88	35.0	1 013	0 0 0	4 385.9	0.1565	1.0000	2.2	7 C	08.7 08.7	1.0 0 0.1	606 1.000	0 17.1	1.006	20	. 50 95 12 12 12	5.8 U.176	51 1.0000 52 1 0000	5 (* 7 (*	000.1
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	8	00 35.9	1.013		2 201 5	0.1526	0000		4 4	3.01	138.7 0.1	565 1.000	0 18.5	1.006) -	04 430	9.7 0.173	31 1.0000	5.9	1.000
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	ğ	00 36.8	1.014	• • •	5 400.9	0.1516	1.0000	2.9 0.9	37 5	3.13 4	43.6 0.1	524 1.000	0 19.8	1.007	5	.12 44:	3.9 0.170	00 1.0000	6.4	1.000
$ \begin{array}{ $	8	00 38.6	1.014	7 0.5	0 403.5	0.1490	1.0000	3.3 0.9	9 9 86	3.21	48.6 0.1	501 1.000	0 20.6	1.007	6 1	20 448	3.6 0.166	59 1.0000	7.0	1.001
$ \begin{array}{ $	8	000 38.4	1.014	8 0.5	4 409.4	0.1473	1.0000	3.6 0.9	. 7 . 7	3.30	53.6 0.1	478 1.000	0 21.5	1.007	7 1	. 25 454	1.8 0.16	53 1.0000	7.4	1.001
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	õ	39.2	1.015	9 0.5	7 414.4	0.1456	1.0000	3.9 0.9	8 8	3.39	158.6 0.1	449 1.000	0 22.5	1.008	8	. 34 460	0.0 0.162	21 1.0000	8.1	1.001
$ \begin{array}{ $	ō	000 43.0	1.015	10 0.6	1 419.6	0.1438	1.0000	4.2 0.9	98 96	3.46 4	163.4 0.1	438 1.000	0 23.1	1.008	9	41 465	5.1 0.15	97 1.0000	8.6	1.002
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0	000 43.5	1.016	11 0.6	6 423.9	0.1417	1.0000	4.6 0.9	2 : 8	3.56	169.1 U.I	407 1.000	0 24.4	1.008	10	49 469	9.6 0.156	57 1.0000	9.3	1.002
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0	000 45.4	1.016	12 0.7	1 429.0	0.1396	1.0000	5.0 0.9	66 11 :	3.65	75.0 0.1	389 1.000	0 Z5.3	1.009	11	52 47:	3.7 0.156	51 1.0000	9.5	1.002
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	i C	000 46.7	1 017	13 0.7	4 433.9	0.1382	1.0000	5.3 0.9	99 12	3.74	78.8 0.1	362 1.000	0 26.4	1.009	: :	50 175		0000 1 20		1 002
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$, c	V 10		14 0.8	0.439.0	0 1355 3	1.0000	5.8 0.9	99 13	3.88	85.1 0.1	315 1.000	0 28.4	1.010	1					
			1.01/	2 0 0 2 0 2 0	1 444 1	0 1347		0 0 0	14	4.11 4	89.2 0.1	225 1.000	0 32.2	1.011	1.	. / 0 48	or . 0	00 T . 0000		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-	0000 49.5	1.018						15	4.29 4	94.7 0.1	158 1.000	0 35.5	1.011	14 1	.78 488	3.8 0.147	75 1.0000	11.7	1.003
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-	0000 50.5	1.018	16 0.8	8 448.8	0.132/	0000-T	0.0	11	0 26 0	98 8 0 1	153 1 000	- ye	1 012	15 1	.85 490	3.5 0.14	50 1.0000	12.4	1.003
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		0000 52.0	1 019	17 0.9	5 454.5	0.1297	1.0000	7.2 1.00	2 C	5 2				1.015	14	00 000	10 0 0	1 0000	12 8	1 004
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			010 1	18 0.9	9 458.6	0.1279	1.0000	7.6 1.00	23			000.1 001		1.012						
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				19 1.0	5 463.7	0.1257	1.0000	8.2 1.00	2 2 2		1.00.00	114 1.000		710.1		- 70 DC	1. C 0. 14		0.01	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		0.00 2.2 2.2 2.2	020	20 1.1	1 469.7	0.1233	1.0000	8.8 1.00	01 13	80		103 1.000		1.013	18	. 04 202	S.J. 0.13	96 1.0000	14.2	1.004
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	•		1.020	21 1.1	5 474.8	0.1217	1.0000	9.3 1.00	01 ⁵⁰	10.1	1.0 0.01	000 I. 000	0 #1.3	1.013	19 2	13 514	1.5 0.13	1. 1.0000	1.01	1.005
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		9.92	1.021	22 1.2.	1 479.1	0.1196	1.0000	9.9 1.00	 =						20 2	. 23 519	9.5 0.130	39 1.0000	16.1	1.005
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				23 1.2	4 483.8	0.1186	1.0000	10.2 1.00	 	ļ										
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				24 1.2	9 489.6	0.1168	1.0000	10.8 1.00	01 Tab	le A56.										
				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0 1145	1 0000	11 6 1 0			Cottooll.	171	([]							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				67 F	0.04	0.1120			2010	nre;	HOVED	0. 121	(TOW)							
25 11.6 0.010 12.5 0.108 1.000 1.5 1.000 <					7.00C 1	0.1123		12.3 1.0	sol'	vent:	C28H58:	0.339	(mol)							
23 151 Get (a) Table ASI Table ASI Table ASI 30 1.62 513.5 0.1009 16.1 1.000 15.1 1.000 15.1 1.001 16.1 1.003 1.01 1.0				Z7 1.4	6 504.0	0.1106	1.0000	12.9 1.0	2											
$ \begin{array}{c} 20 & 1.58 & 513.6 & 0.1049 & 1.0000 & 15.1 & 1.003 \\ 1.66 & 1011 & 1.11 & 1.003 & 15.1 &$				28 1.5	1 508.7	0.1087	1.0000	13.6 1.0	5											
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				29 1.5	8 513.5	0.1064	1.0000	14.5 1.0	5				54							
Obs Table A54. Table A54. Table A54. 3.22 (suc) solute: Cambra 0.93 (suc) 20.93 (suc)				30 1.6	2 518.6	0.1049	1.0000	15.1 1.00	13 L	<u>م</u>	-	`۔ 	H 12	Pntr						
OS6 (mol) Table A3. Date A3. Solute: Childing: Color (mol) Solute: Childing: Childing: Pint									۲	.	 ;		.		Table	A58.				
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		11-1 23								bar	X .		раг	I			10-11-0	5 100 0		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		(100) 000		lable A5	4.										annios		SHULLHAN	160.0	f Tom	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	2	(lom) 251		solute:	CH3OH:	0	.051 (mol)		- 0	67.0	373.6 0.2	1.000	0 3.0	0.999	solven	: :	C28H58:	0.329 (mol)	
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		0000 25.7	1.003	19 2.00	1 513.7	0.0369 1	0000	53.4 1.00	90 LI	3 57 5	10 8 11	1 1 0000	22.0	1 010	19 1	. 66 51/	1.2 0.150	1.0000	10.7	1.003
				5 i c 1 i c				10.1 F.CC	5	n 10.0	14.8 U.L	441 I. UUU	1 63.0	1.010					; ;	
				1					3	2	17.0 0.11	112 T. UUU		1.010	i					

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0.074 (mol)

Table A59.

C6H130H

solv	ent;	C28H	58:	0.362 (mo	51)	
run	P	T	<u>×</u> 1	у_1	H ^{PS} 12	Pntr
	bar	к	-	-	bar	-
1	0.17	373.5	0.1622	1.0000	1.0	0.996
2	0.18	384.6	0.1616	1.0000	1.1	0.996
3	0.19	383.4	0.1612	1.0000	1.2	0.996
4	0.20	391.3	0.1608	1.0000	1.3	0.996
5	0.22	392.9	0.1602	1.0000	1.3	0.996
6	0.24	400.4	0.1595	1.0000	1.5	0.996
7	0.25	405.3	0.1591	1.0000	1.5	0.996
8	0.27	408.1	0.1580	1.0000	1.7	0.997
9	0.28	413.8	0.1578	1.0000	1.8	0.997
10	0.30	420.2	0.1569	1.0000	1.9	0.997
11	0.34	423.1	0.1555	1.0000	2.1	0.997
12	0.36	428.7	0.1546	1.0000	2.3	0.997
13	0.37	434.1	0.1545	1.0000	2.4	0.997
14	0.40	440.2	0,1535	1.0000	2.5	0.997
15	0.43	446.6	0. 1523	1.0000	2.8	0.997
16	0.46	448.5	0.1512	1.0000	3.0	0.997
17	0.47	452.7	0.1509	1.0000	3.1	0.998
18	0.51	461.5	0.1493	1.0000	3.4	0. 998
19	0.56	466.9	0.1477	1.0000	3.7	0.998
20	0.58	470.7	0.1471	1.0000	3.9	0.998
21	0.61	475.4	0.1460	1.0000	4.1	0.998
22	0.66	481.1	0.1443	1.0000	4.5	0.998
23	0.70	485.8	0.1430	1.0000	4.8	0.999
24	0.73	489.9	0.1419	1.0000	5.1	0.999
25	0.78	496.4	0.1404	1.0000	5.4	0.999
26	0.81	500.5	0.1393	1.0000	5.7	0.999
27	0.85	505.1	0.1382	1.0000	6.0	0.999
28	0.88	509.1	0.1372	1.0000	6.3	0.999
29	0.92	513.2	0.1359	1.0000	6.6	1.000
30	0.95	517.1	0.1348	1.0000	6.9	1.000

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Tabl	e A60.								
solu	te;	H2O:	H2O: 0.061 (mol)						
solv	ent;	C28H	58:	0.339 (mol)					
run	P	T	<u>×</u> 1	у ₁	H ^{PS} 12	Pntr			
	bar	ĸ	-	-	bar	-			
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	1.52 1.64 1.75 1.80 1.85 1.95 1.98 2.02 2.06 2.11 2.206 2.27 2.31 2.37 2.31 2.37 2.47 2.53	428 8 434.4 438.6 443.8 449.3 454.9 459.4 463.6 468.9 473.8 473.8 473.8 473.8 473.8 478.9 473.8 548.6 494.4 498.5 504.5 508.6 513.8 519.0	0.0696 0.0638 0.0583 0.0563 0.0546 0.0547 0.0518 0.0499 0.0499 0.0499 0.0435 0.0435 0.0435 0.0435 0.0422 0.0395 0.0377 0.0363 0.0363	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	21.7 25.4 29.7 31.5 33.9 37.1 38.6 40.0 41.4 44.1 50.0 53.6 53.1 55.3 59.1 63.3 67.1 72.2	1.001 1.001 1.002 1.002 1.002 1.002 1.002 1.002 1.002 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.004 1.004			

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